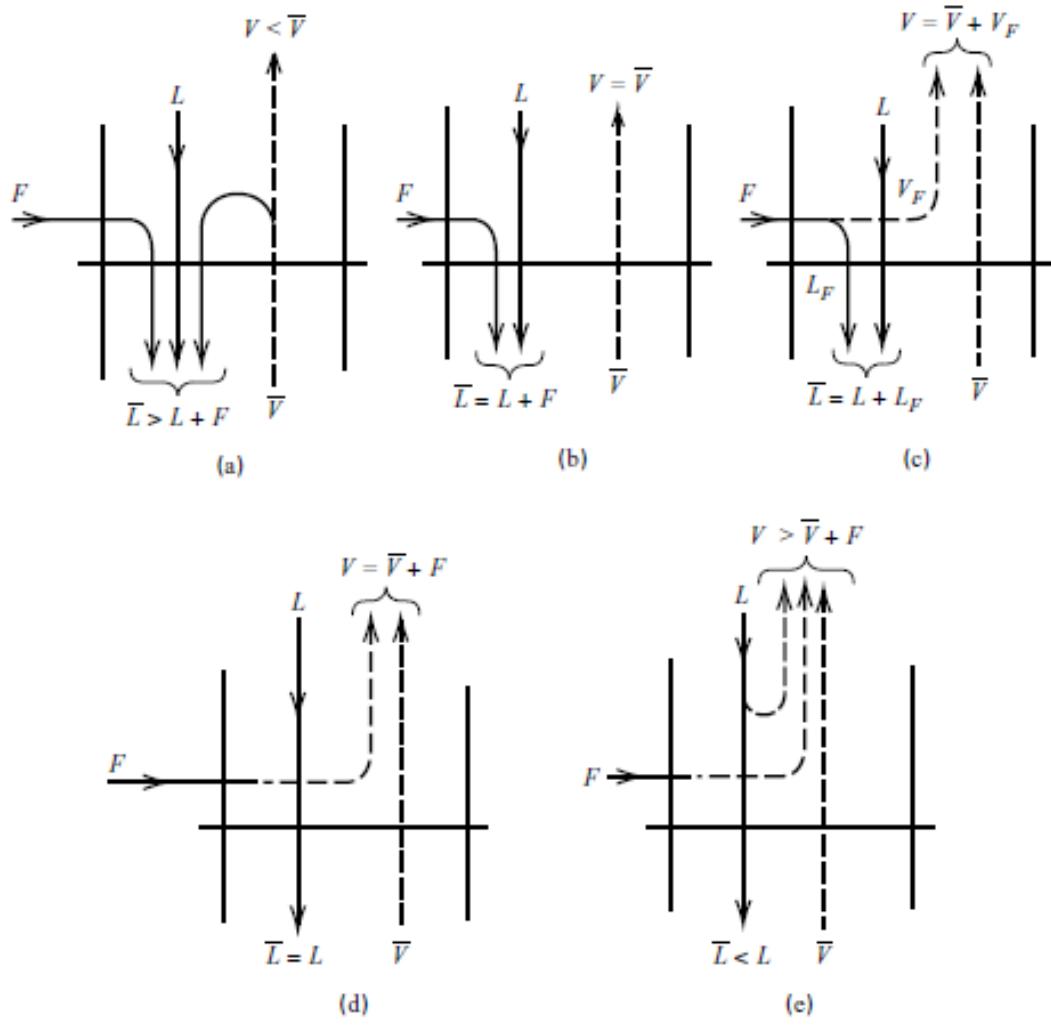
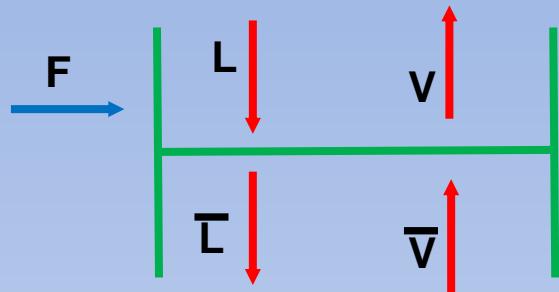


Fondamenti delle operazioni unitarie dell'industria chimica

Distillazione - parte seconda







$$F + L + \bar{V} = \bar{L} + V$$

$$FH_F + LH_L + \bar{V}H_V = \bar{L}H_L + VH_V$$

$$(\bar{L} - L)H_L = (\bar{V} - V)H_V + FH_F$$

$$q = \frac{(\bar{L} - L)}{F} = \frac{H_V - H_F}{H_V - H_L}$$

$$\frac{(\bar{L} - L)H_L}{F} = \frac{(\bar{V} - V)H_V}{F} + H_F$$

$$\frac{(\bar{L} - L)H_L}{F} = \frac{(\bar{L} - L)H_V}{F} + H_F - H_V$$

$$\frac{(\bar{L} - L)}{F} = \frac{H_V - H_F}{H_V - H_L}$$

$$q = \frac{(\bar{L} - L)}{F} = \frac{H_v - H_F}{H_v - H_L}$$

Calore necessario a portare 1 mole di feed a vapore saturo

Calore latente molare di vaporizzazione

$$q = \frac{(\bar{L} - L)}{F} = \frac{H_v - H_F}{H_v - H_L}$$

Liquido sottoraffreddato

$$q > 1$$

Liquido saturo

$$q = 1$$

Liquido + vapore

$$1 > q > 0$$

Vapore saturo

$$q = 0$$

Vapore surriscaldato

$$q < 0$$

T_F, H_F

$$q = \frac{(L - L)}{F} = \frac{H_v - H_f}{H_v - H_l}$$

Liquido sottoraffreddato

$$q > 1$$

Liquido saturo

$$q = 1$$

Liquido + vapore

$$1 > q > 0$$

Vapore saturo

$$q = 0$$

Vapore surriscaldato

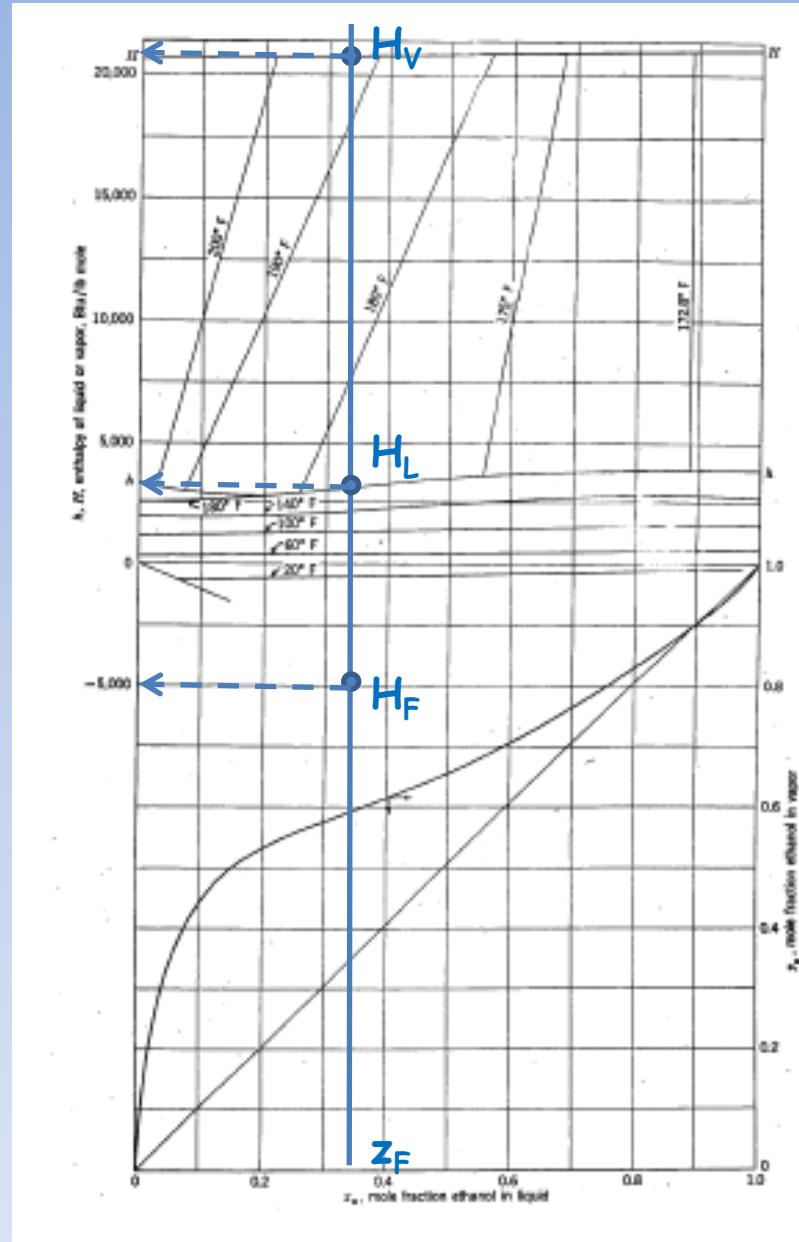
$$q < 0$$

$$H_f = -5000$$

$$H_l = 3120$$

$$H_v = 20700 \quad (BTU/lbmol)$$

$$q = \frac{20700 - (-5000)}{20700 - 3120} = \frac{25700}{17580} = 1.461$$

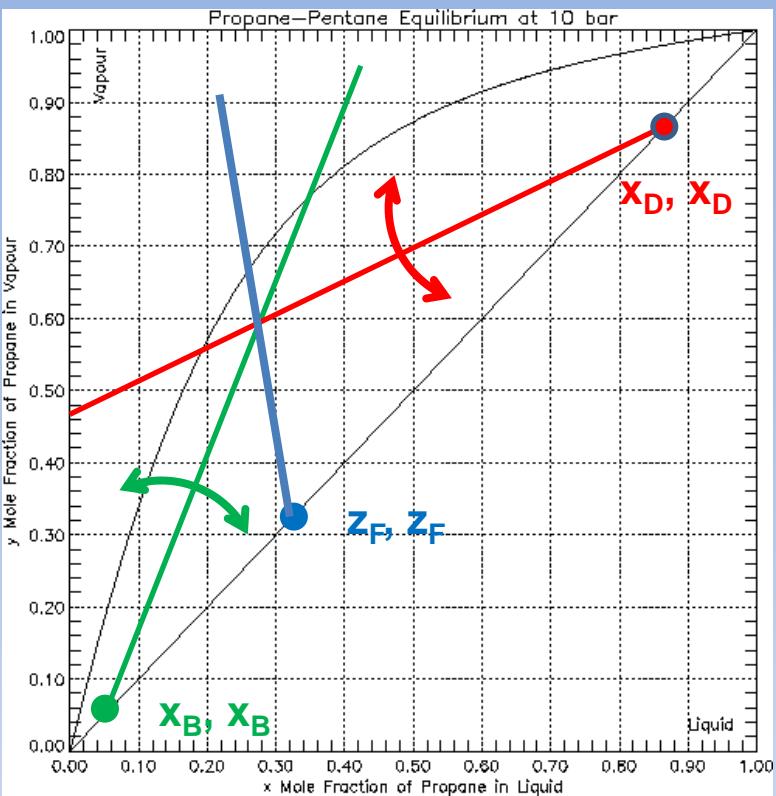


$$yV = Lx + Dx_D$$

$$y\bar{V} = \bar{L}x - Bx_B$$

$$(\bar{V} - V)y = (\bar{L} - L)x - (Bx_B + Dx_D)$$

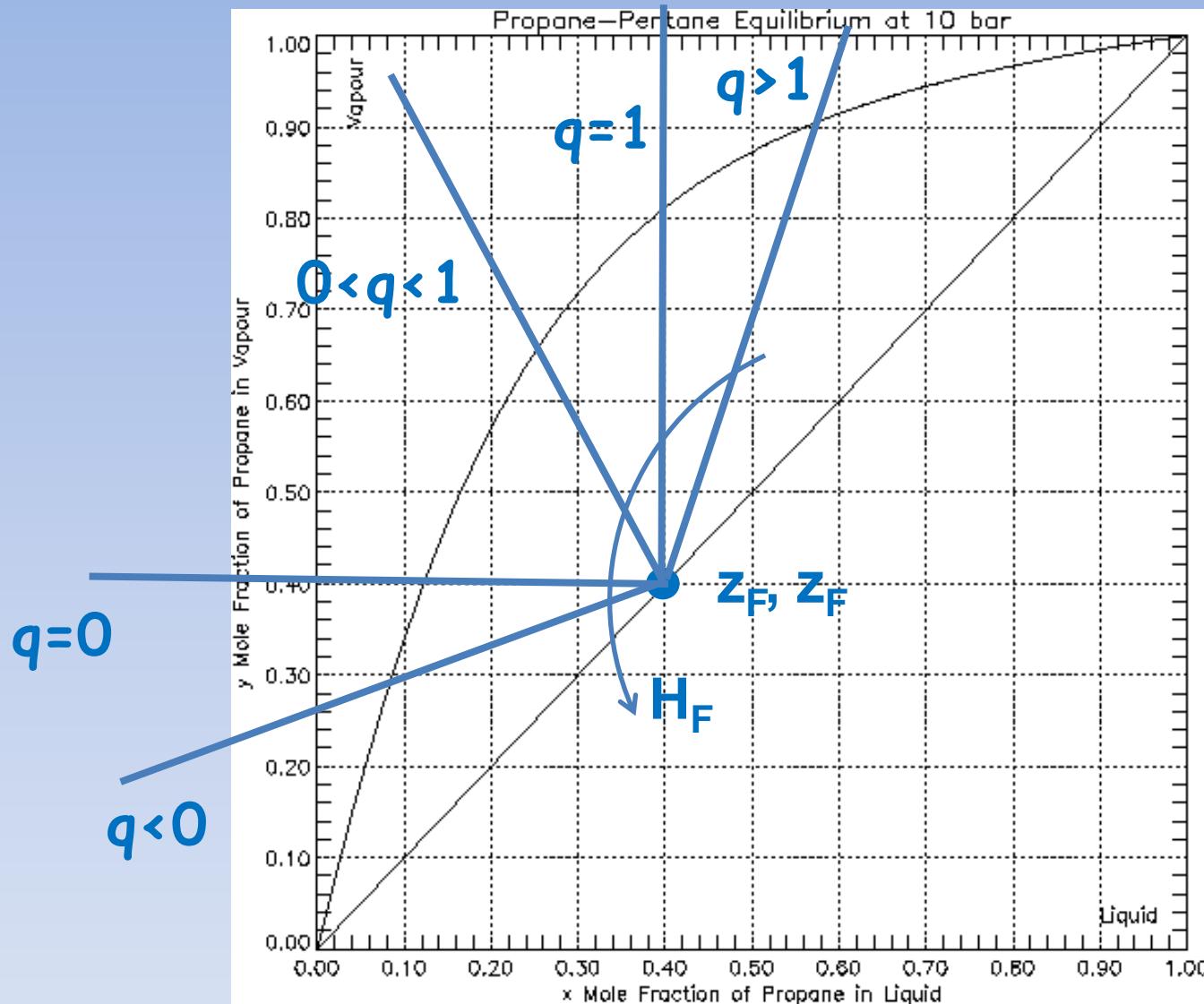
$$y = \frac{q}{q-1}x - \frac{z_F}{q-1}$$

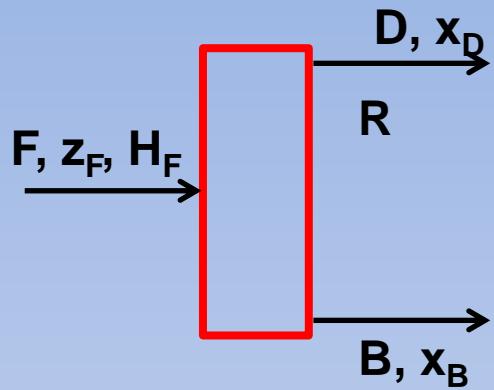


$$(\bar{L} - L) = Fq$$

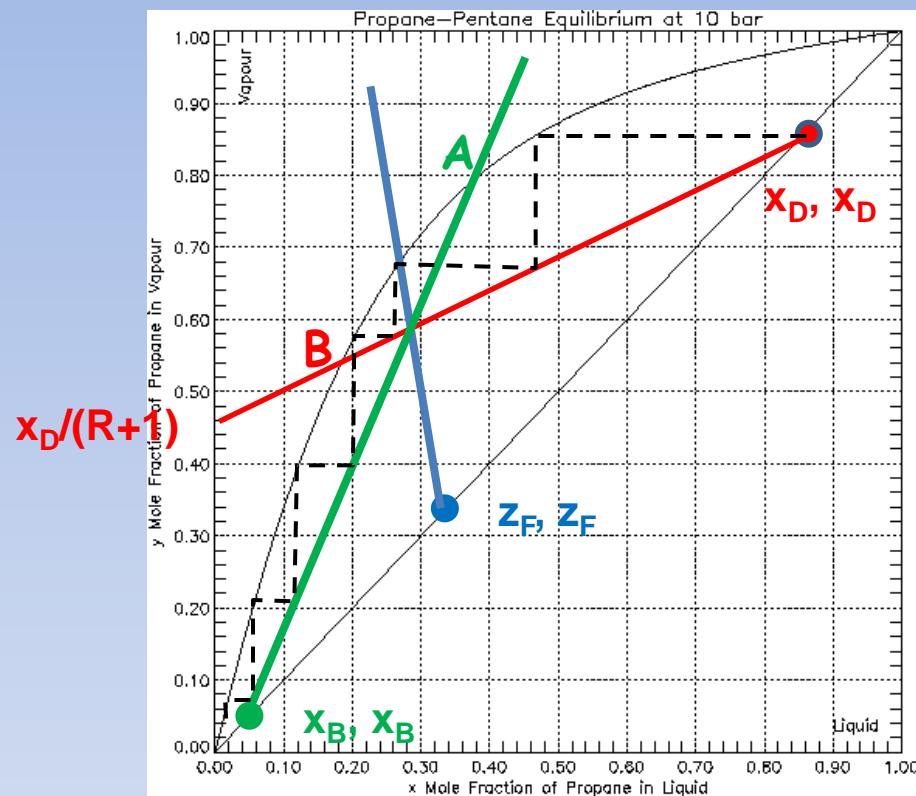
$$(\bar{V} - V) = F(q-1)$$

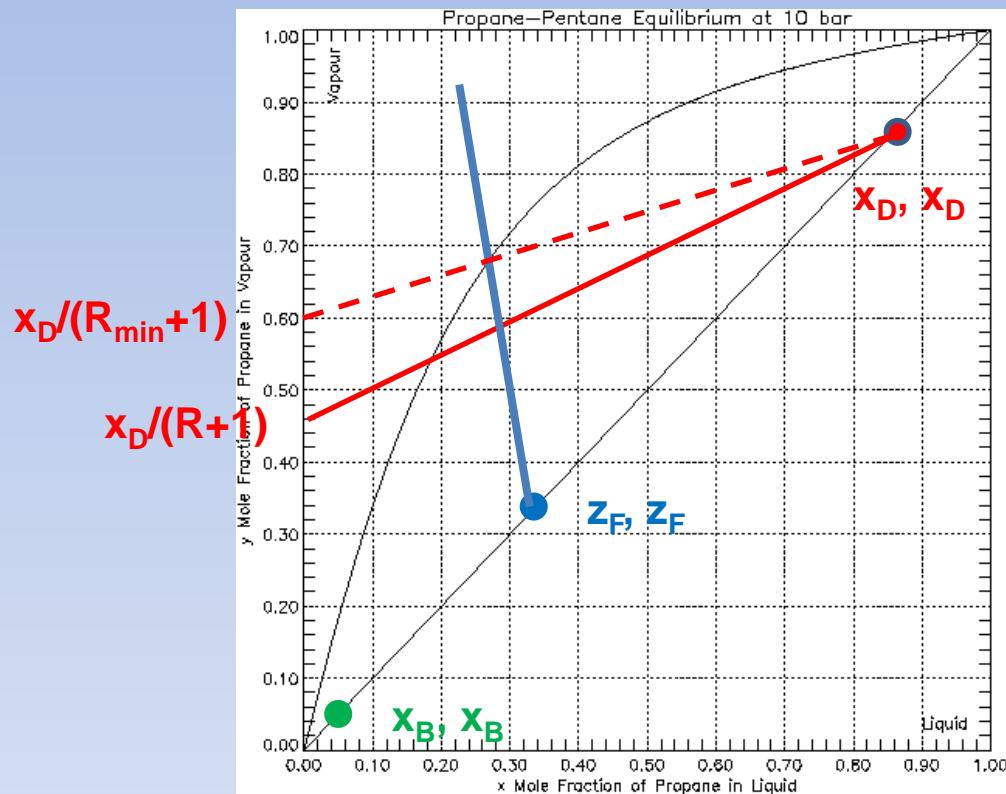
$$(Bx_B + Dx_D) = Fz_F$$





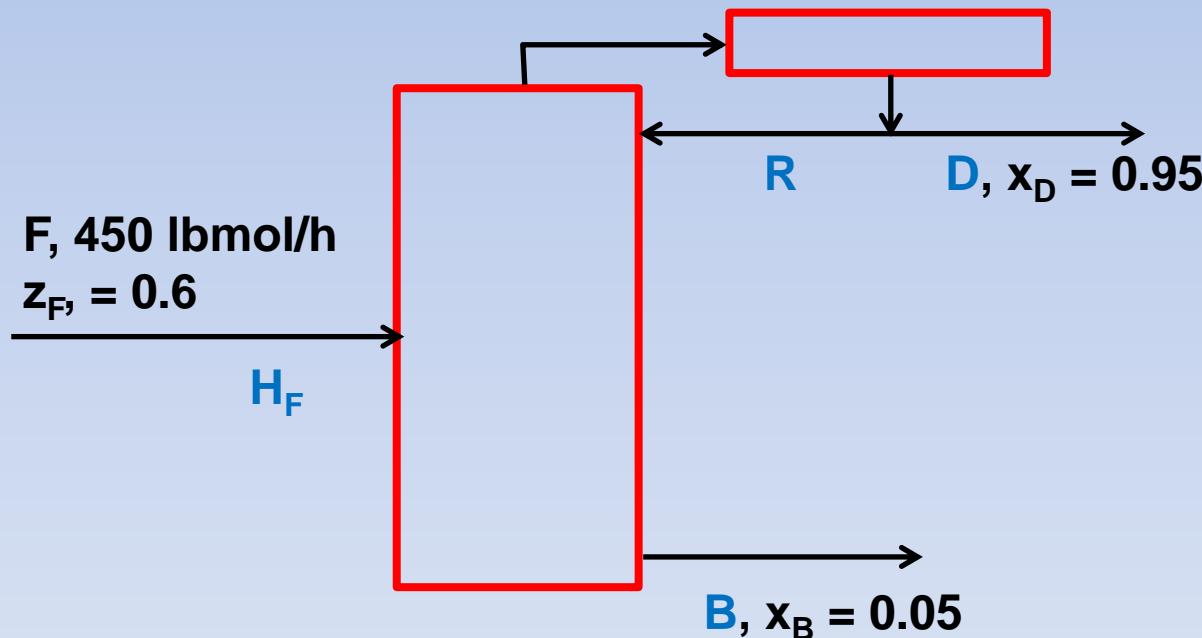
$N_P = 6$
Feed al terzo piatto





Esercitazione numerica n. 3 – Distillazione

2) Four hundred and fifty lbmol/h of a mixture of 60 mol% benzene and 40 mol% toluene is to be separated into a liquid distillate and a liquid bottoms product of 95 mol% and 5 mol% benzene, respectively. The feed enters the column with a molar per-cent vaporization equal to the distillate-to-feed ratio. Use the McCabe-Thiele method to compute, at 1 atm: N_{\min} , R_{\min} , and N for $R/R_{\min} = 1.3$, and the optimal feed-stage location.



$$1) F = D + B$$

$$2) Fz_F = Dx_D + Bx_B$$

$$1) 450 = D + B$$

$$2) 270 = 0.95D + 0.05B$$

$$22.5 = 0.05D + 0.05B$$

$$270 = 0.95D + 0.05B$$

$$247.5 = 0.9D$$

$$D = 275 \text{ lbmol/h}; B = 175 \text{ lbmol/h}$$

$$D/F = 0.611 = \text{vaporizzato/feed}$$

$$H_F = H_L + 0.611(H_v - H_L)$$

$$H_v - H_F = H_v - H_L - 0.611(H_v - H_L)$$

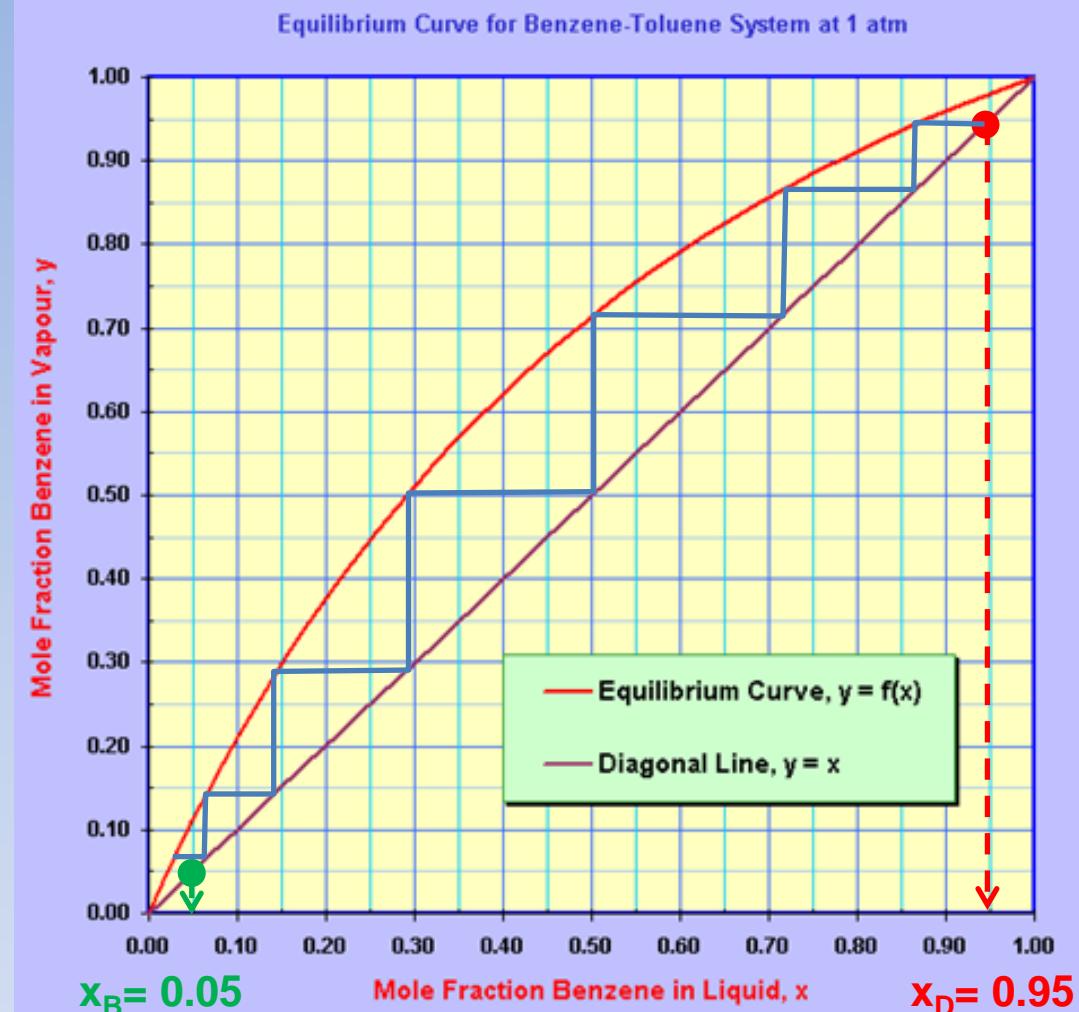
$$H_v - H_F = 0.389(H_v - H_L)$$

$$q = 0.389$$

$$q/(q-1) = -0.637$$

$$y = -0.637x + 0.981$$

$N_{\min} = 7$



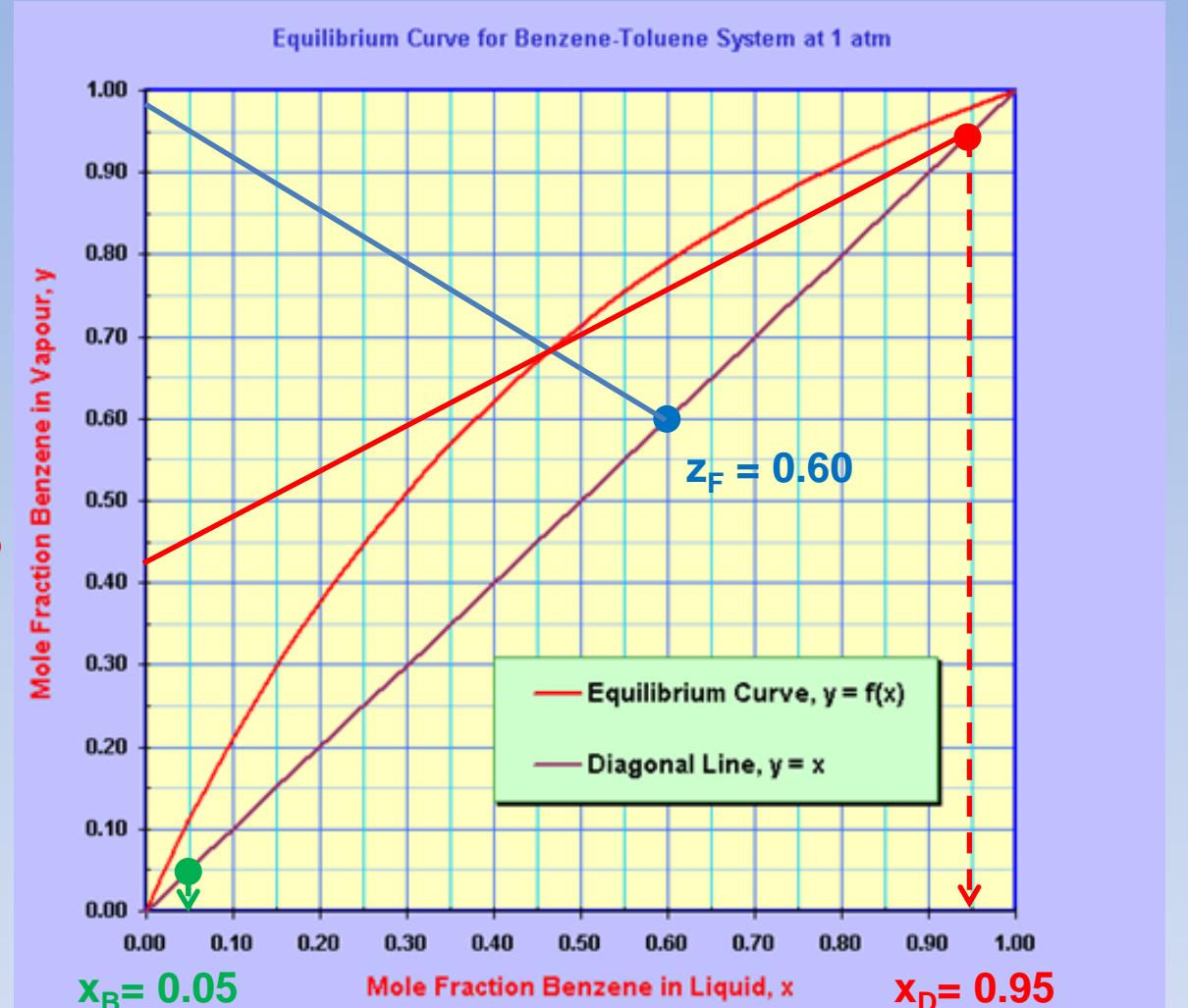
$$N_{\min} = 7$$

$$Y = -0.637x + 0.981$$

$$x_D/(R_{\min} + 1) = 0.425$$

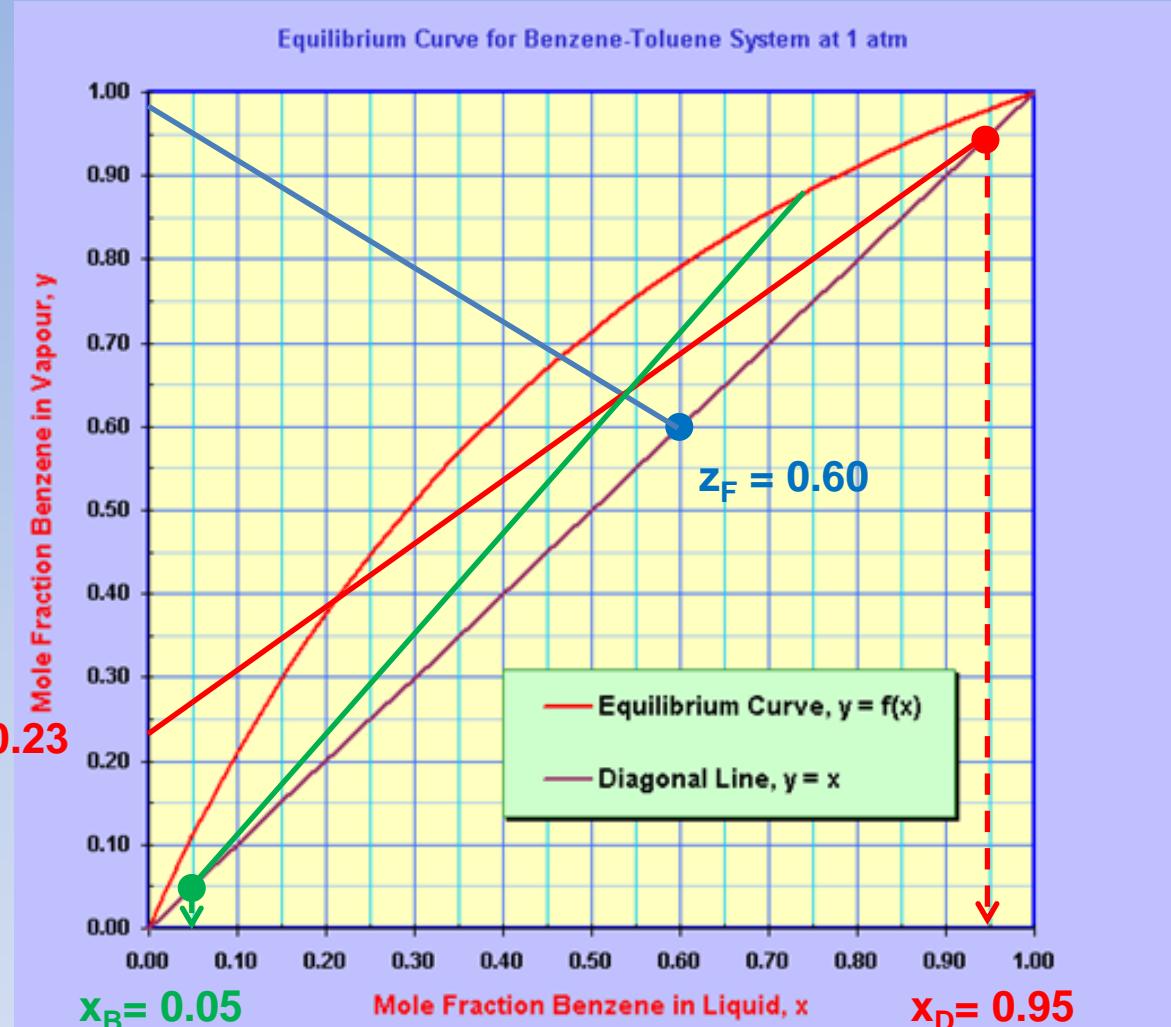
$$R_{\min} = 1.23$$

$$R = 1.3R_{\min} = 1.6$$



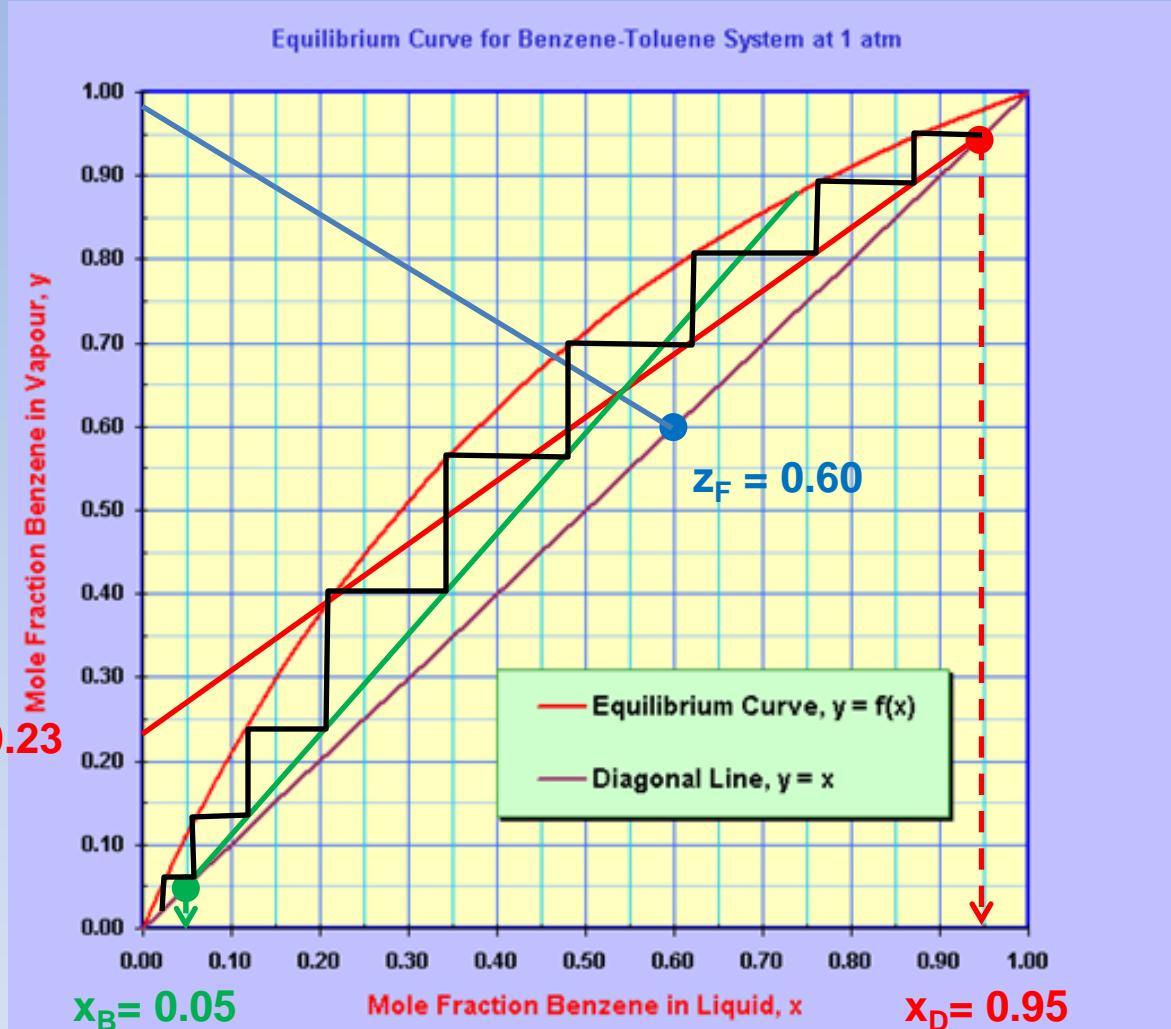
$$R = 1.3R_{\min} = 1.6$$

$$x_D/(R + 1) = 0.23$$



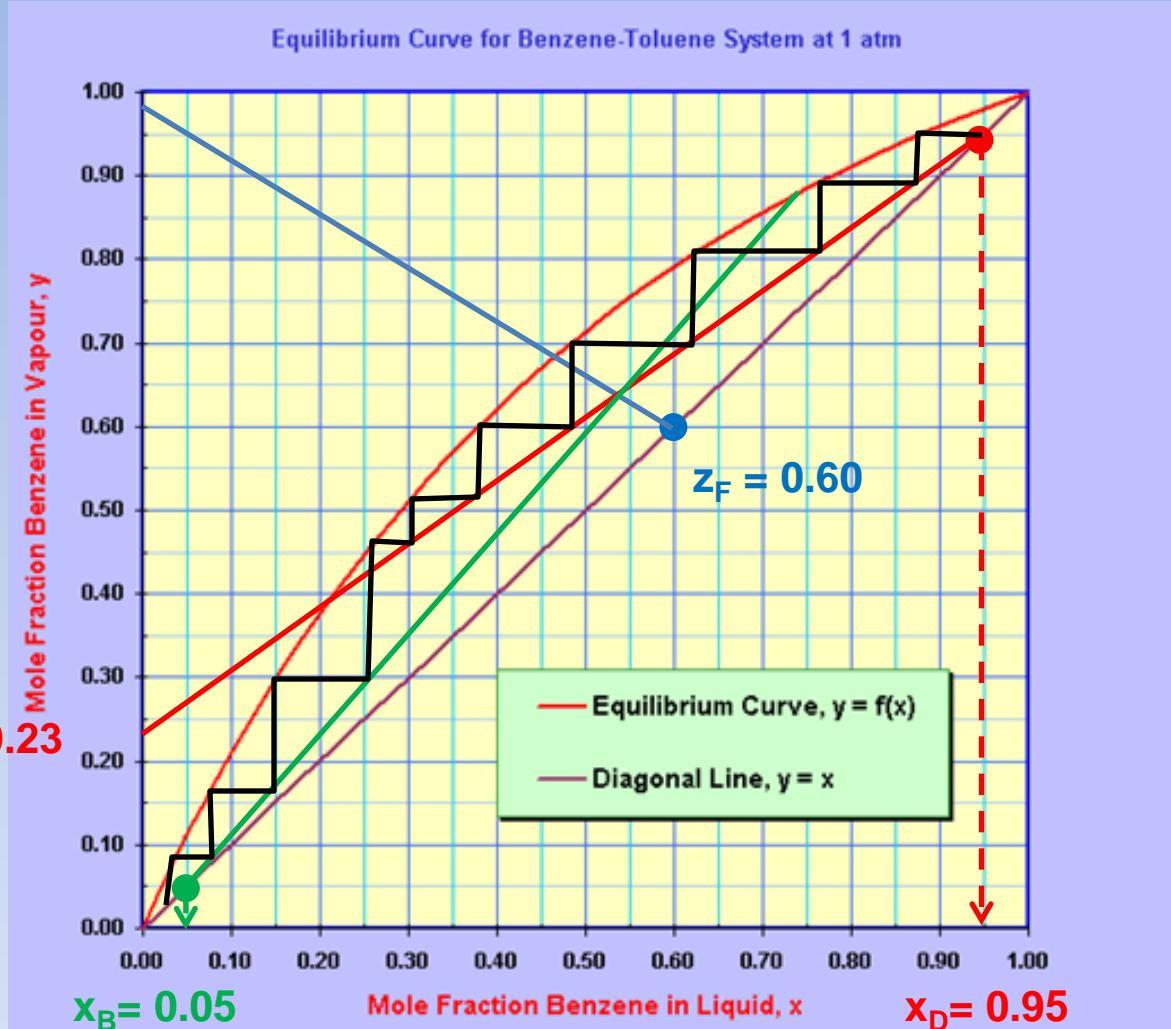
$N_p = 9$
Feed at 4°

$$x_D/(R + 1) = 0.23$$



$N_p = 10$
Feed at 7°

$$x_D/(R+1) = 0.23$$



$N_p = 9$
Feed at 3°

$$x_D/(R+1) = 0.23$$

