

# Homeostatic states and relaxed configurations of a spherical thick shell

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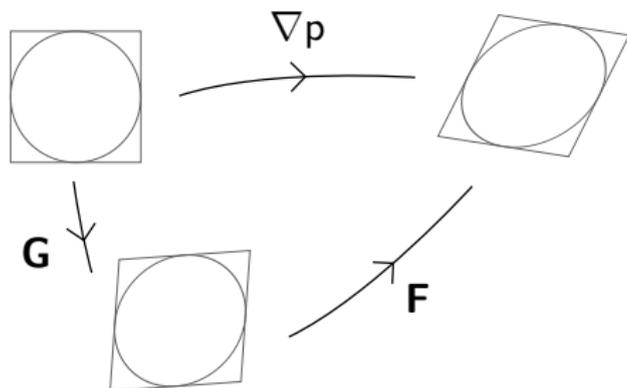
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*A joint work with:*

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# Kröner-Lee scheme



$$\mathbf{F} := \nabla p \mathbf{G}^{-1}$$

# Spherically symmetric shapes

Transplacement

$$\mathbf{p}(\mathbf{x}, \tau) = \mathbf{x}_o + \rho(\xi, \tau) \mathbf{e}_r(\vartheta, \varphi),$$

Transplacement gradient and remodeling

$$\nabla \mathbf{p}|_{\mathbf{x}} = \rho'(\xi) \mathbf{P}_r + \xi^{-1} \rho(\xi) \mathbf{P}_h$$

$$\mathbf{G}(\mathbf{x}) = \gamma_r(\xi) \mathbf{P}_r + \gamma_h(\xi) \mathbf{P}_h$$

Effective stretch

$$\mathbf{F}(\mathbf{x}) := \nabla \mathbf{p}|_{\mathbf{x}} \mathbf{G}(\mathbf{x})^{-1} = \lambda_r(\xi) \mathbf{P}_r + \lambda_h(\xi) \mathbf{P}_h$$

# General setting

Effective stretches

$$\lambda_h(\xi) := \frac{\rho(\xi)}{\xi \gamma_h(\xi)}, \quad \lambda_r(\xi) := \frac{\rho'(\xi)}{\gamma_r(\xi)}$$

Jacobian determinant

$$J_p(\xi) := (\rho(\xi)/\xi)^2 \rho'(\xi)$$

Relaxed Jacobian

$$J(\xi) := \gamma_h^2(\xi) \gamma_r(\xi)$$

Balance

$$2 (S_r(\xi) - S_h(\xi)) + \xi S_r'(\xi) = 0$$

$$S_r(\xi_{\mp}) = -\pi_{\mp}$$

$\pi_{\mp}$  outer *reference* pressure.

# General setting

Cauchy stress

$$\mathbb{T}_h(\xi) = \frac{\rho(\xi)}{\xi} S_h(\xi) / J_\rho(\xi), \quad \mathbb{T}_r(\xi) = \rho'(\xi) S_r(\xi) / J_\rho(\xi)$$

Balance equations

$$\frac{\rho(\xi)}{\xi} \left( 2 (\mathbb{T}_r(\xi) - \mathbb{T}_h(\xi)) \rho'(\xi) + \rho(\xi) \mathbb{T}'_r(\xi) \right) = 0$$

$$\mathbb{T}_r(\xi_\mp) = -\hat{p}_\mp$$

$\hat{p}_\mp$  outer *actual* pressure

$$\pi_\mp = (\rho(\xi_\mp) / \xi_\mp)^2 \hat{p}_\mp$$

# Strain energy function

Elastically incompressible material

$$\lambda_h^2(\xi)\lambda_r(\xi) = 1 \quad (1)$$

Fung strain energy function

$$\phi(\lambda_h) = \frac{c}{H} \left( -1 + e^{\frac{1}{2}\Gamma(\lambda_h^2-1)^2} \right) \quad (2)$$

Because of the incompressibility constraint the response function turns out to be defined only for the deviatoric part of the stress:

$$\mathbf{T}_h(\xi) - \mathbf{T}_r(\xi) = \frac{\lambda_h(\xi)}{2} \phi'(\lambda_h(\xi)) \quad (3)$$

# Initial homeostatic state

*For a given shape and fixed values of the outer pressure, find the stress and the transformation stretch. It is assumed that the hoop stress field is uniform across the thickness.*

*Results: It is shown that there exists only one solution (although no formal proof is given). The main point is that the transplacement is the identity map. This also makes Piola stress and Cauchy stress indistinguishable.*

# Initial homeostatic state

The reference shape is the same as the given shape:

$$\rho(\xi) = \xi \quad \Rightarrow \quad \lambda_h \gamma_h = 1, \quad \lambda_r \gamma_r = 1$$

We assume that a homeostatic state is characterized by a uniform hoop stress  $S_h^\diamond$ . The balance equation gives the following solution for the radial stress

$$S_r(\xi) = S_h^\diamond + \frac{C}{\xi^2}$$

By enforcing the two boundary conditions

$$S_r(\xi_{\mp}) = -\pi_{\mp}$$

we get both  $C$  and  $S_h^\diamond$

Piola stress field

$$S_r(\xi) = \frac{\pi_+ (\xi^2 - \xi_-^2) \xi_+^2 + \pi_- (\xi_+^2 - \xi^2) \xi_-^2}{\xi^2 (\xi_-^2 - \xi_+^2)}$$

$$S_h^\diamond = \frac{\pi_+ \xi_+^2 - \pi_- \xi_-^2}{(\xi_-^2 - \xi_+^2)}$$

# Initial homeostatic state

## Numerical values

$$\xi_m = 2000/20 \mu\text{m}$$

$$L = H/1.18^2 \mu\text{m}$$

$$c = 0.8769 \times 10^{-6} \times 10^{-1} \text{ N } \mu\text{m}^{-2} = 876.9 \times 10^{-1} \text{ kPa}$$

$$\Gamma = 12.99$$

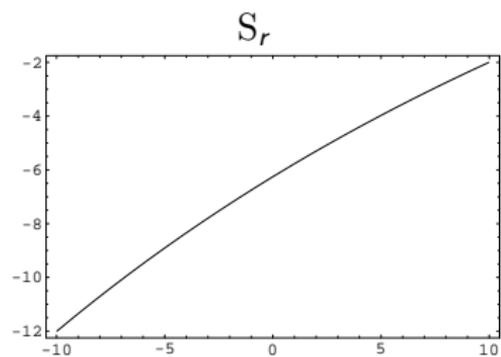
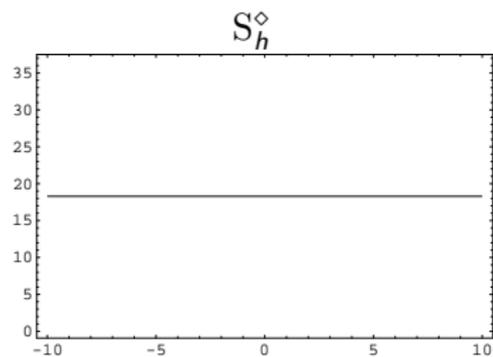
$$H = 27.8 \mu\text{m}$$

$$\pi_+ = 2 \times 10^{-9} \text{ N } \mu\text{m}^{-2} = 2 \text{ kPa}$$

$$\pi_- = 12 \times 10^{-9} \text{ N } \mu\text{m}^{-2} = 12 \text{ kPa}$$

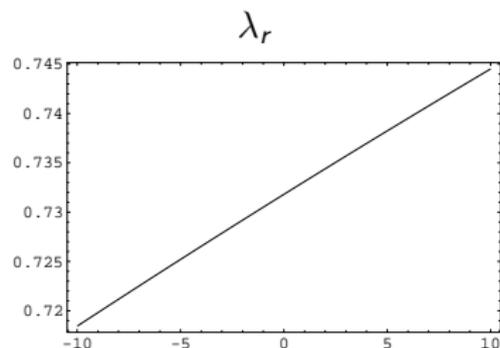
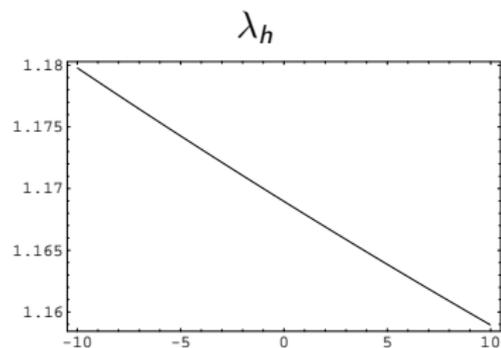
# Initial homeostatic state

Stress



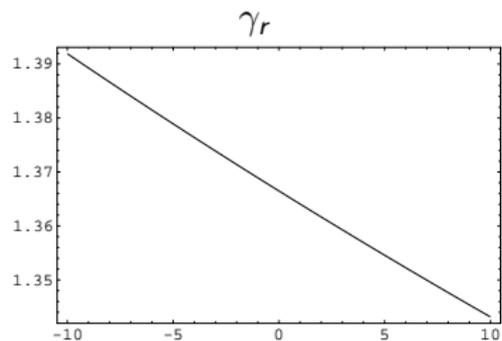
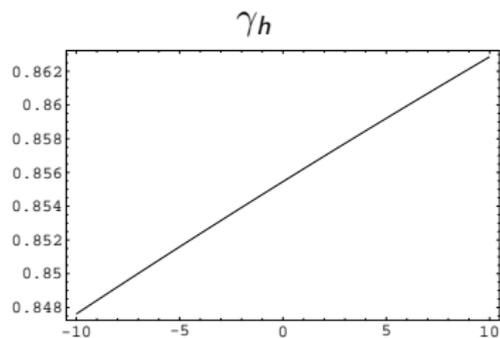
# Initial homeostatic state

## Effective stretch



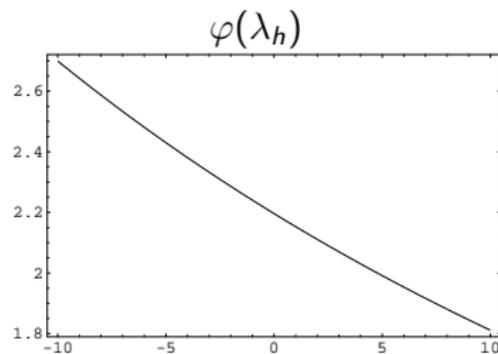
# Initial homeostatic state

## Transformation stretch



# Initial homeostatic state

Strain energy density



# Unloaded shape

*After setting the outer pressure to zero, let the body relax while keeping the transformation stretch unchanged.*

*Results: The configuration the body reaches is not stress free.*

## Unloading transplacement

Since both  $\gamma_h$  and  $\gamma_r$  are left unchanged the transplacement is isochoric. From

$$\lambda_h(\xi) = \frac{\rho(\xi)}{\xi \gamma_h(\xi)}, \quad \lambda_r(\xi) = \frac{\rho'(\xi)}{\gamma_r(\xi)}, \quad \lambda_h^2(\xi) \lambda_r(\xi) = 1$$

we get

$$\rho(\xi) = (\xi^3 + (\rho_m^3 - \xi_m^3))^{1/3} \quad (4)$$

where  $\rho_m := \rho(\xi_m)$  is an integration constant.

From material response and balance equation

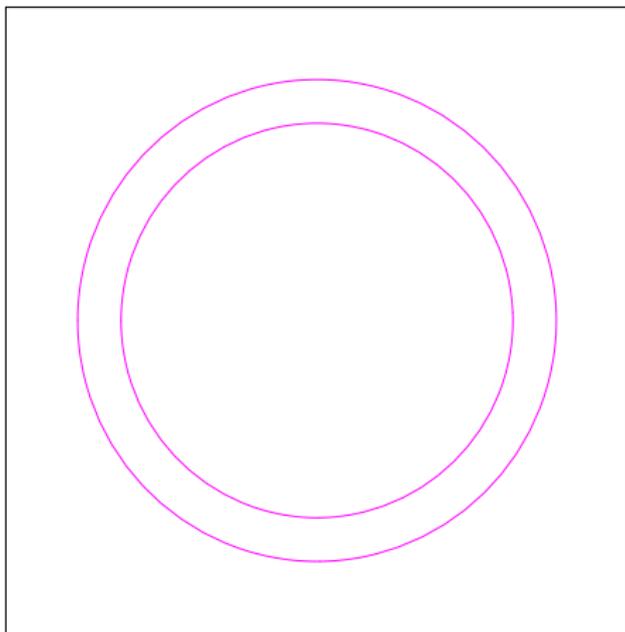
$$\begin{aligned}T_h(\xi) - T_r(\xi) &= \frac{\lambda_h(\xi)}{2} \phi'(\lambda_h(\xi)) \\2 (T_r(\xi) - T_h(\xi)) \rho'(\xi) + \rho(\xi) T_r'(\xi) &= 0\end{aligned}$$

we get the boundary value problem

$$\begin{aligned}-\lambda_h(\xi) \phi'(\lambda_h(\xi)) \rho'(\xi) + \rho(\xi) T_r'(\xi) &= 0 \\T_r(\xi_{\mp}) &= 0\end{aligned}$$

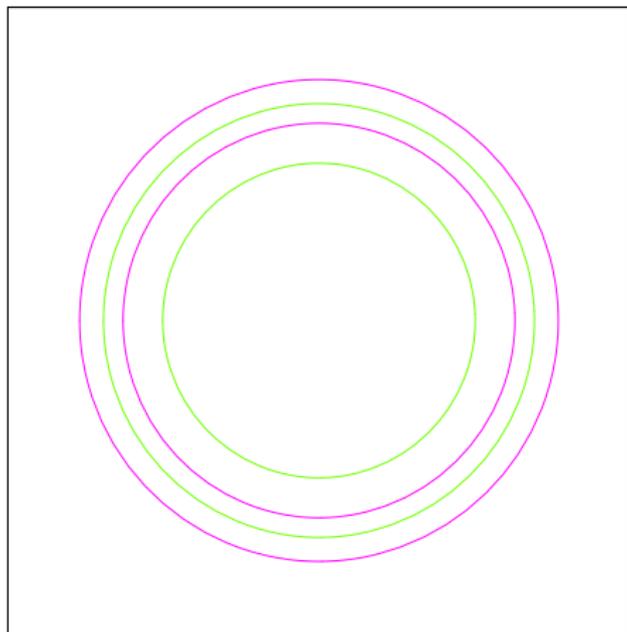
which we can solve (possibly numerically) for both  $T_r$  and  $\rho_m$ , by using also  $\lambda_h(\xi) := \rho(\xi)/\xi \gamma_h(\xi)$ . Finally we compute  $T_h$ .

# Reference shape



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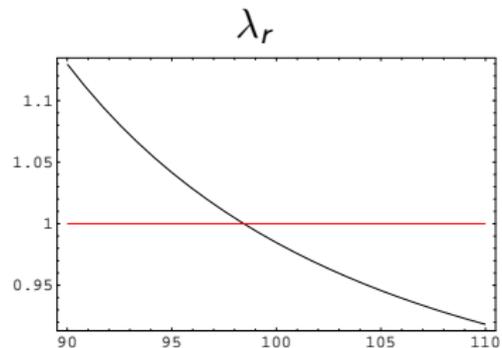
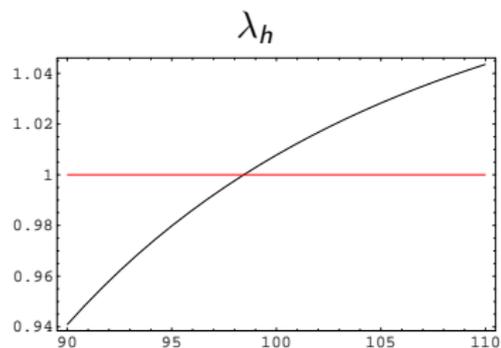
# Unloaded shape



[automatically generated figure]

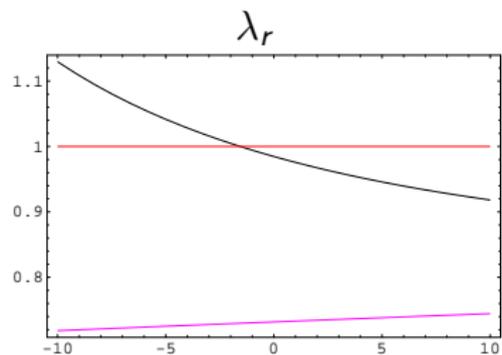
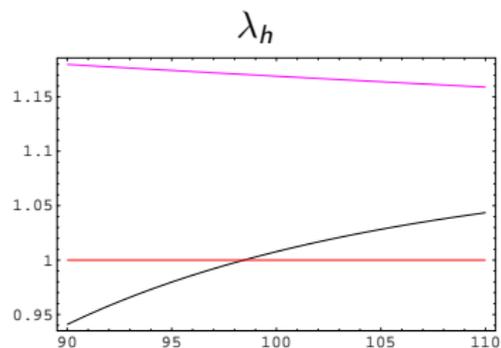
# Unloaded shape

## Residual effective stretch



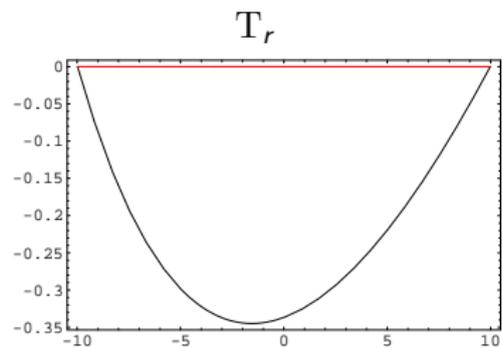
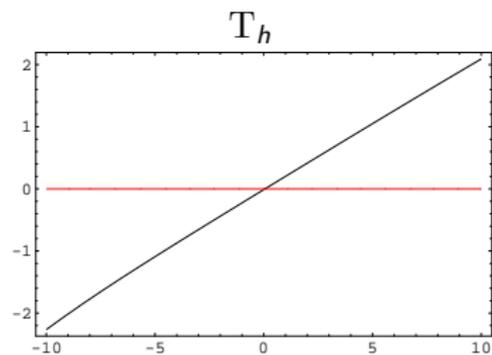
# Unloaded shape

## Residual effective stretch



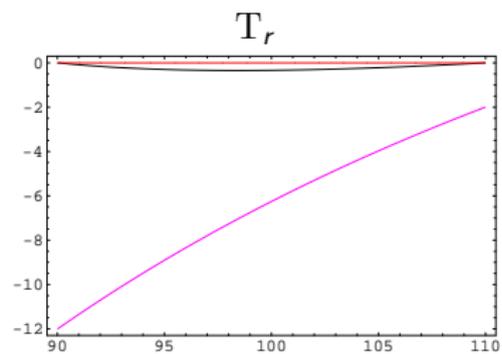
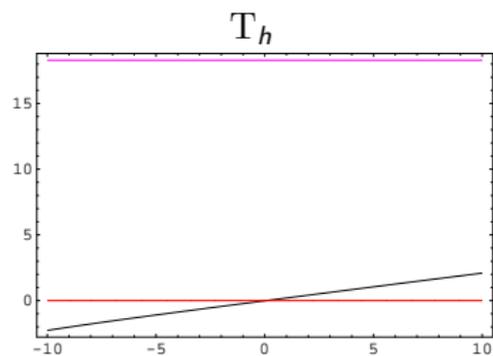
# Unloaded shape

## Residual stress

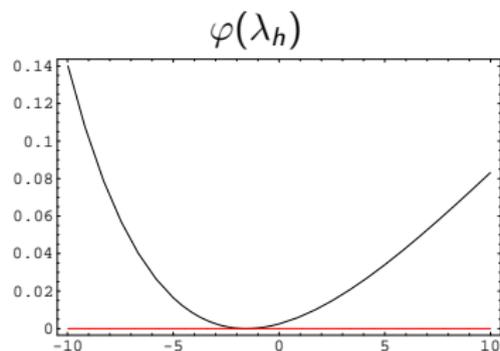


# Unloaded shape

## Residual stress

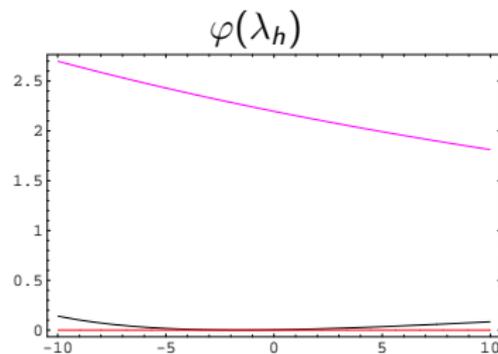


Residual strain energy density



# Unloaded shape

Residual strain energy density



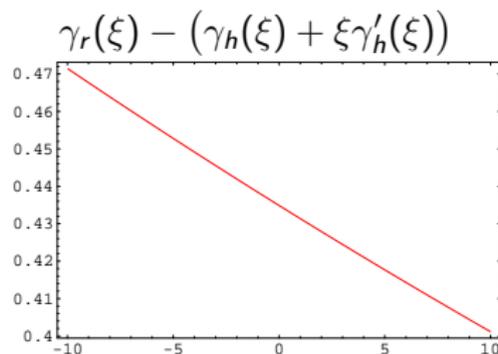
# Relaxed configuration

Does a relaxed configuration exist?

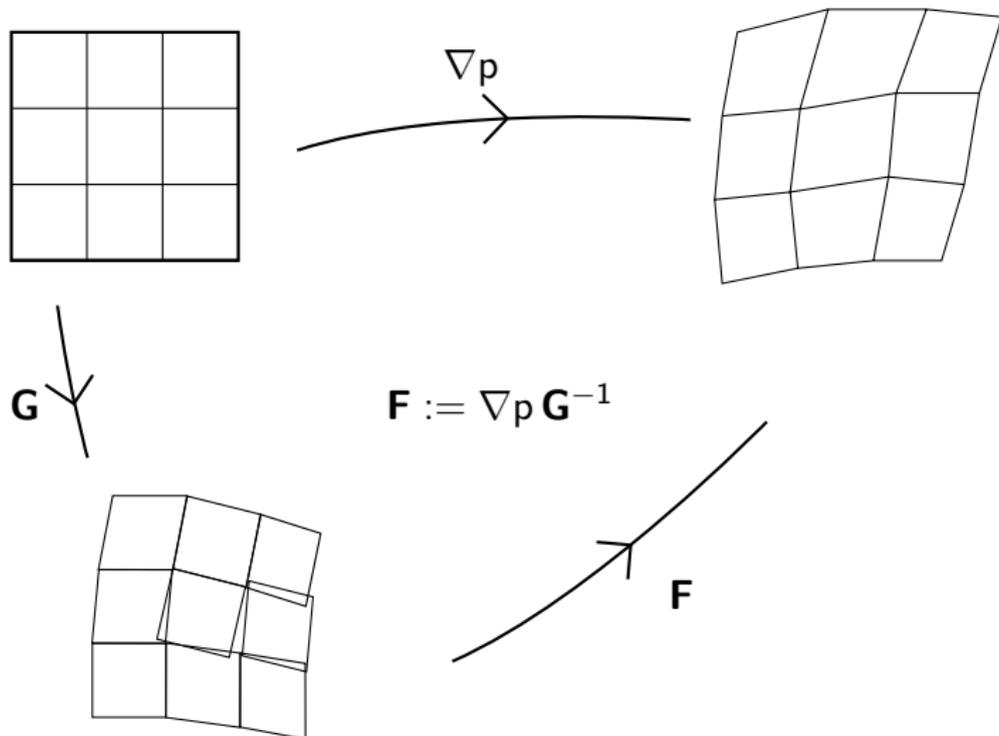
$$\nabla p|_x = \rho'(\xi) \mathbf{P}_r + \xi^{-1} \rho(\xi) \mathbf{P}_h$$

$$\lambda_r(\xi) = \frac{\rho'(\xi)}{\gamma_r(\xi)}, \quad \lambda_h(\xi) = \frac{\rho(\xi)}{\xi \gamma_h(\xi)}$$

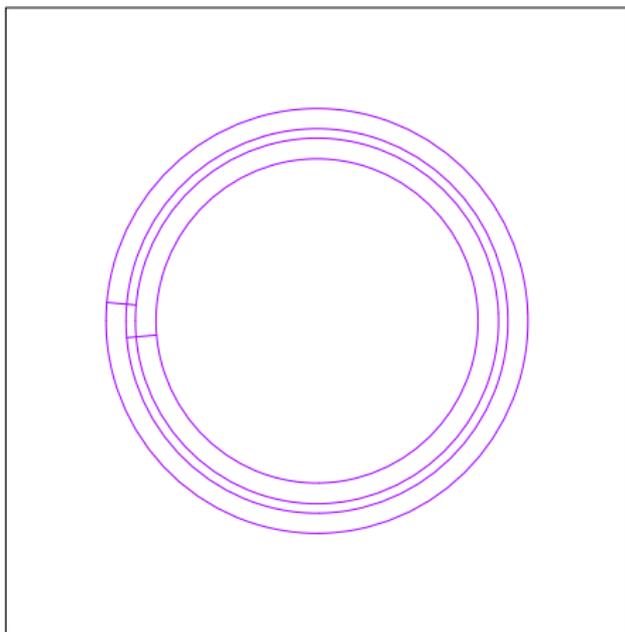
$$\lambda_r(\xi) = 1 \ \& \ \lambda_h(\xi) = 1 \quad \Rightarrow \quad \gamma_r(\xi) - (\gamma_h(\xi) + \xi \gamma_h'(\xi)) = 0$$



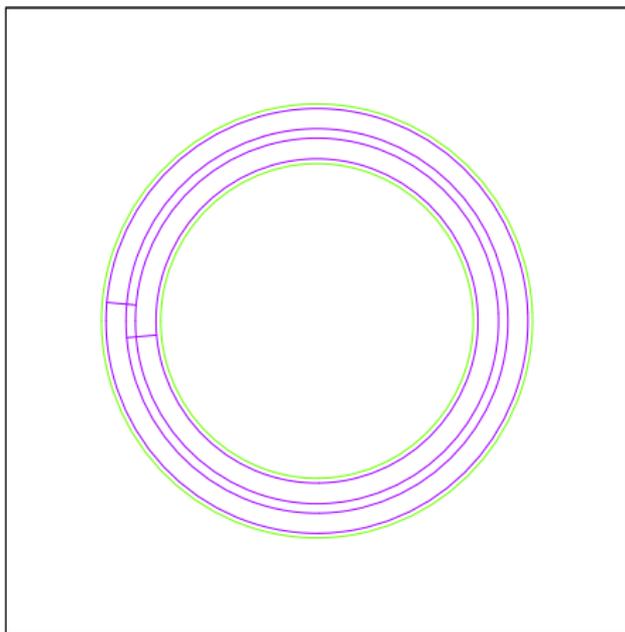
# Kröner-Lee scheme



# Unloaded two layer shape

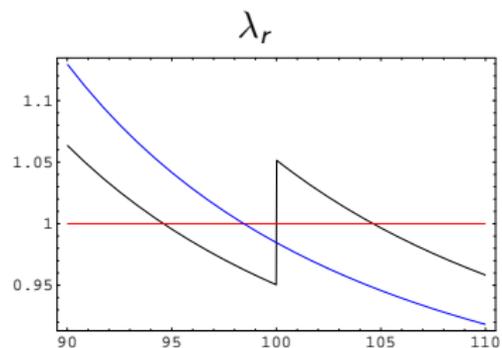
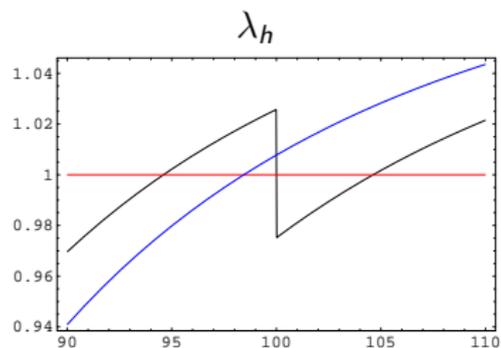


# Unloaded two layer shape



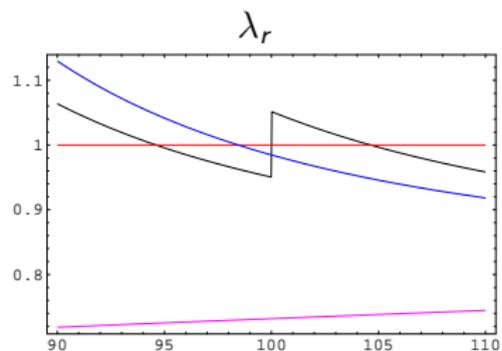
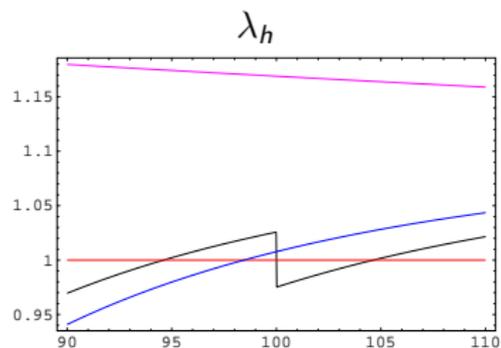
# Unloaded two layer shape

## Residual effective stretch



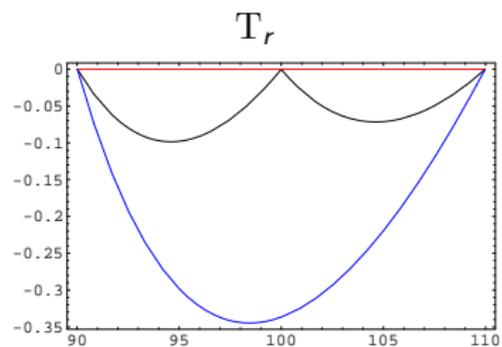
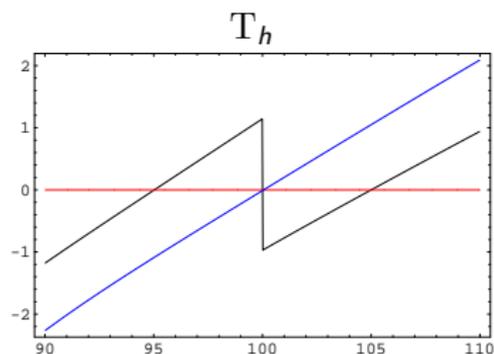
# Unloaded two layer shape

## Residual effective stretch



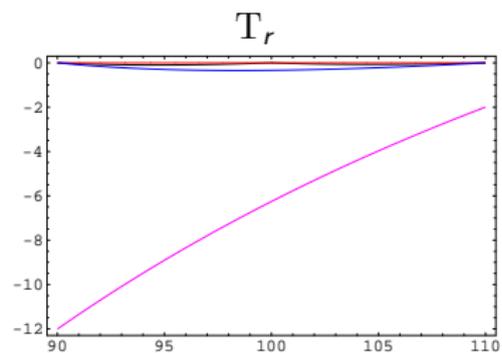
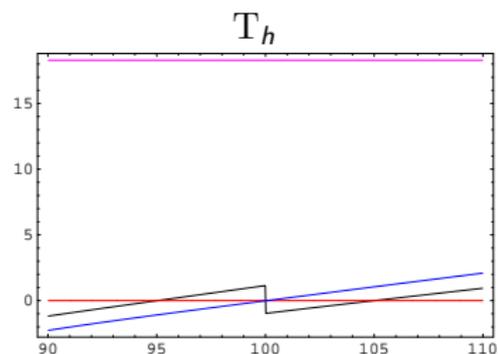
# Unloaded two layer shape

## Residual stress



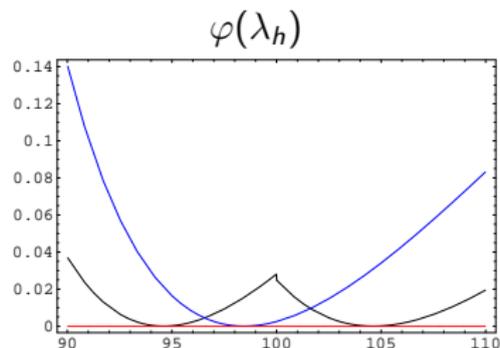
# Unloaded two layer shape

## Residual stress



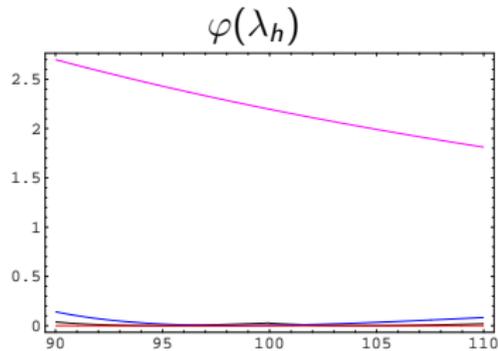
# Unloaded two layer shape

Residual strain energy density



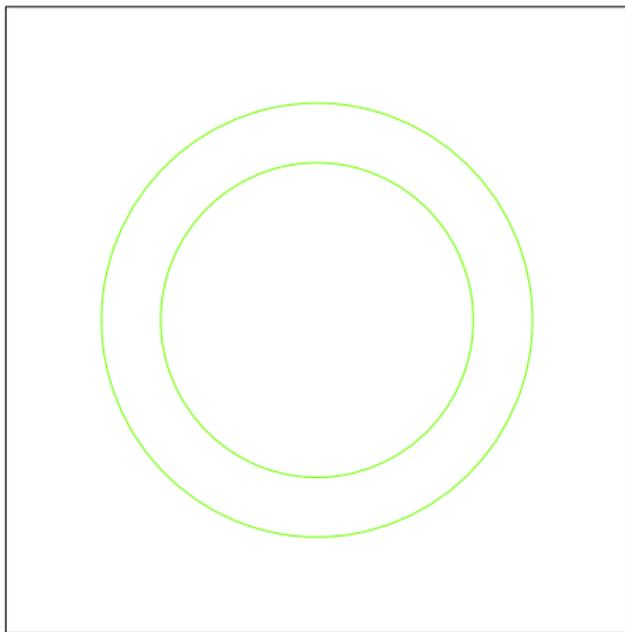
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Residual strain energy density

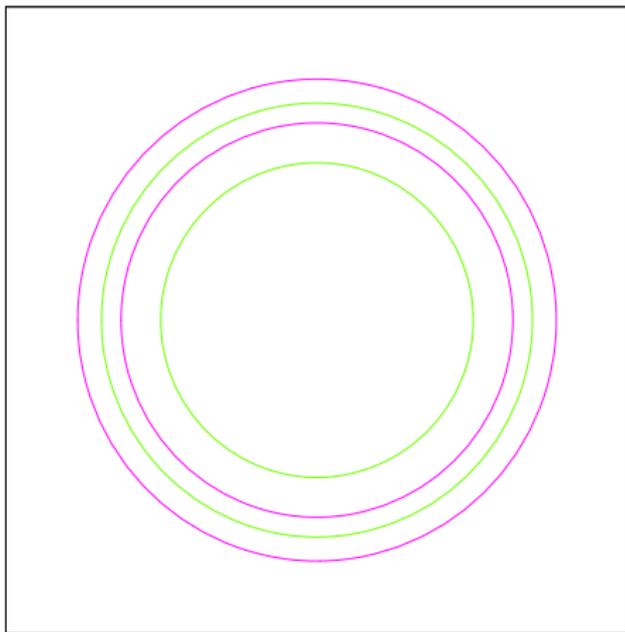




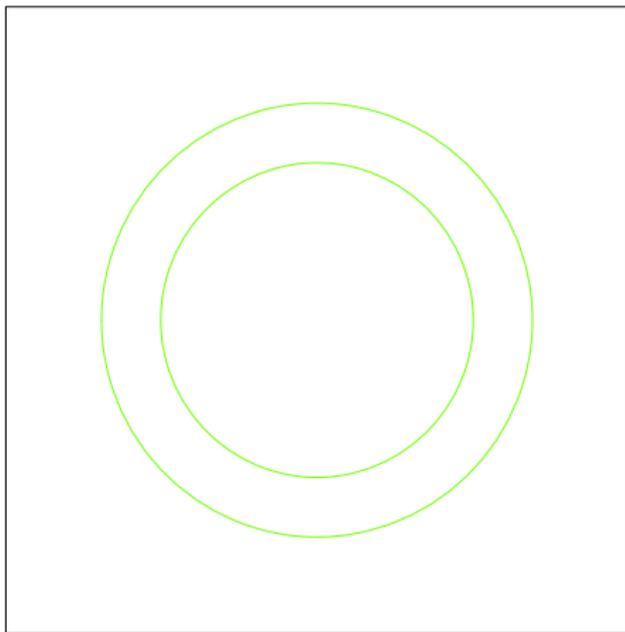
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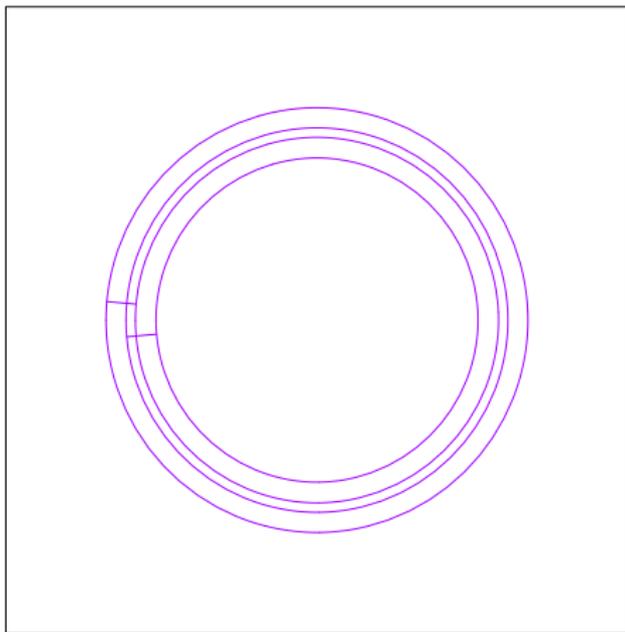
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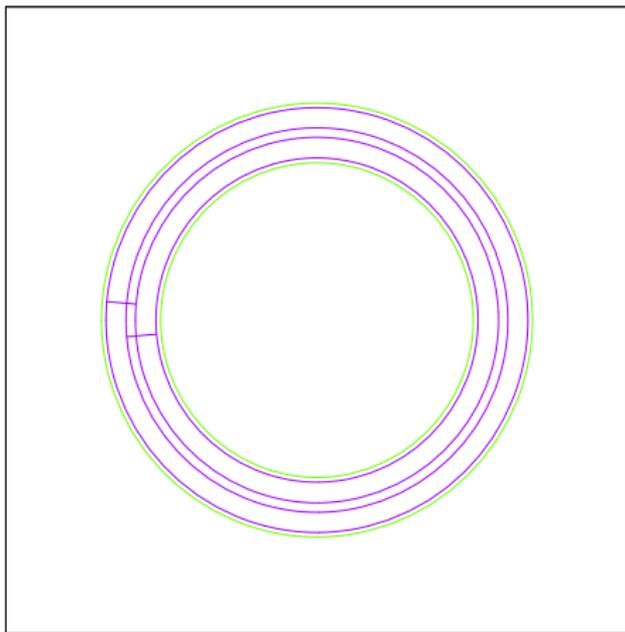
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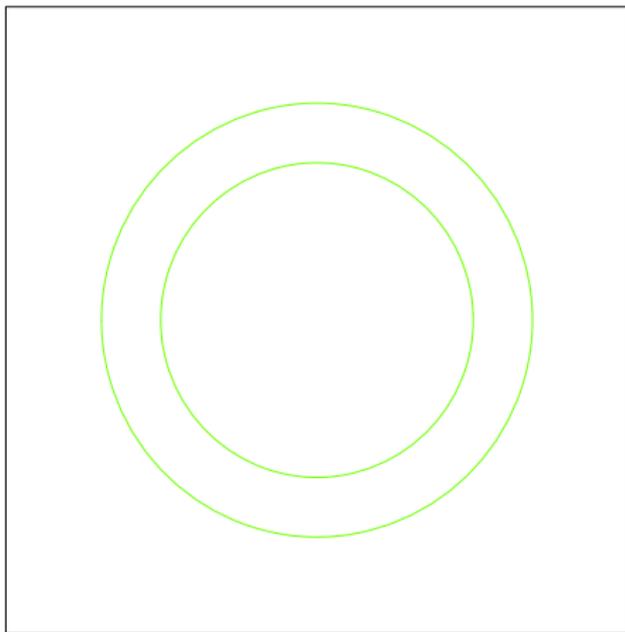
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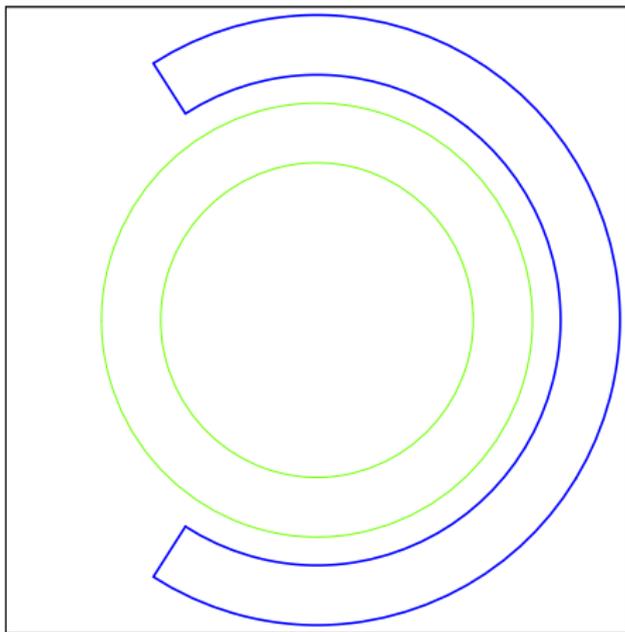
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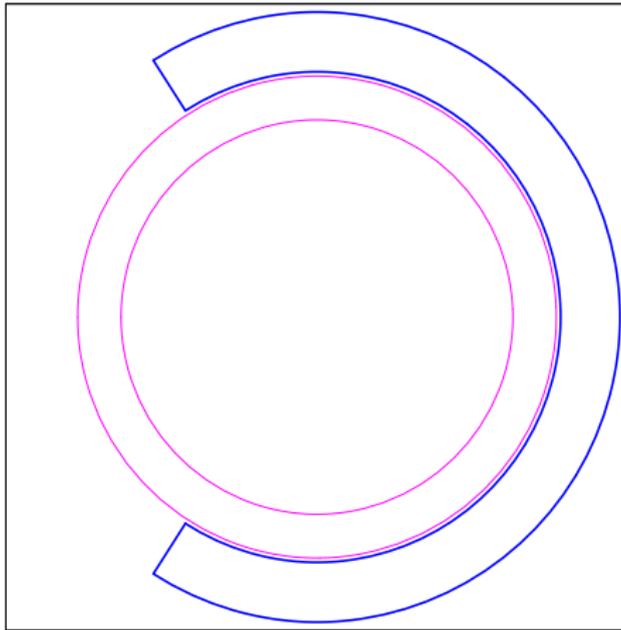
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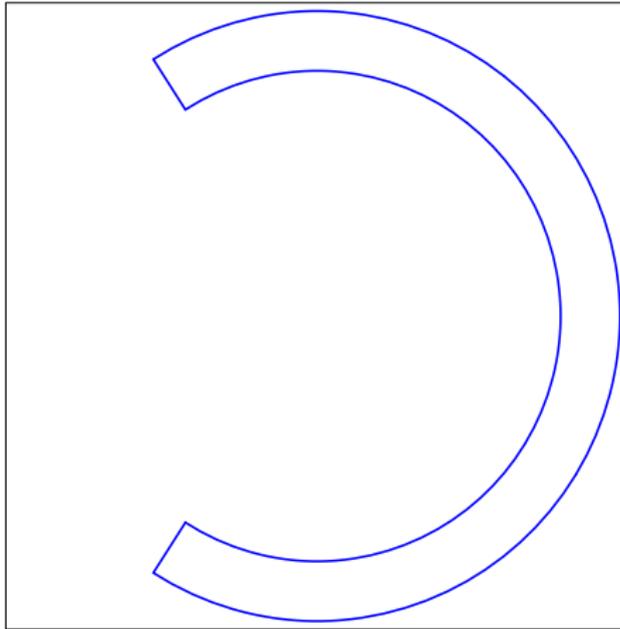
Open slice



Open slice



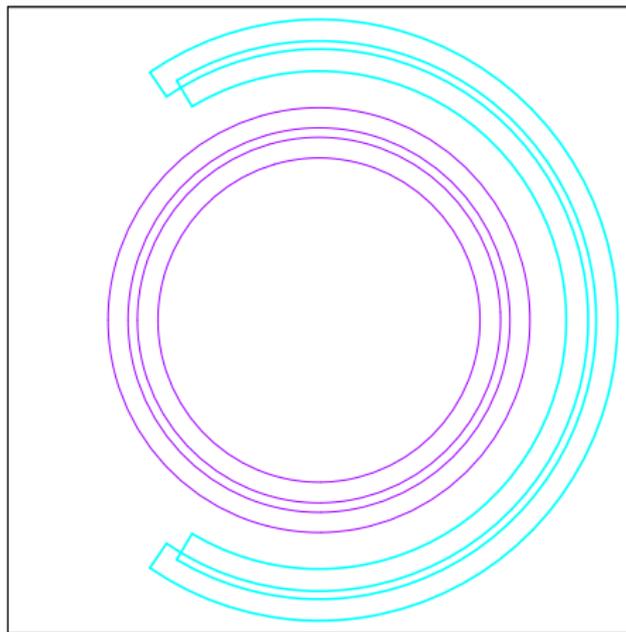
Open slice



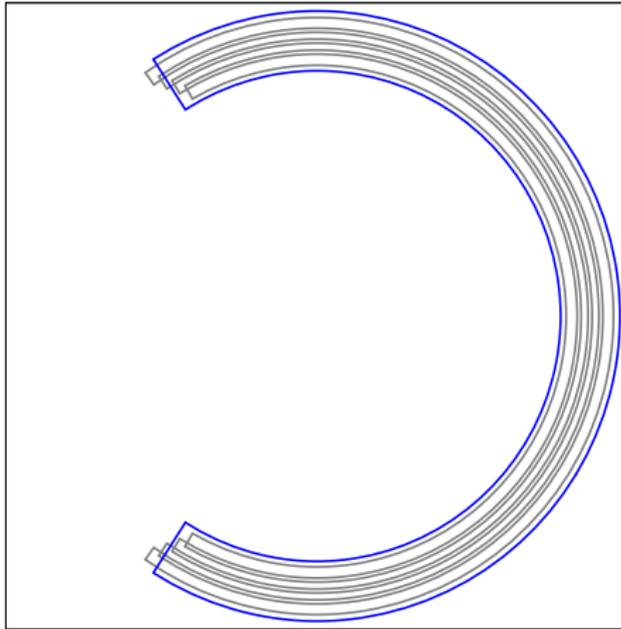




Open slice split into 2 layers



Open slice split into 4 layers



Open slice split into 6 layers

