

Rigid and affine motions

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1 Motions

By *motion of a body* \mathcal{B} we mean a regular function

$$\mathfrak{p} : \mathcal{B} \times \mathbb{R} \rightarrow \mathcal{E} \quad (1)$$

such that for any t

$$\mathfrak{p}(\cdot, t) : \mathcal{B} \rightarrow \mathcal{E} \quad (2)$$

is a placement and

$$\mathfrak{p}_A(\cdot) \equiv \mathfrak{p}(A, \cdot) : \mathbb{R} \rightarrow \mathcal{E} \quad (3)$$

is the motion of any body point A . Hence a motion is a one-parameter family of placements. A motion can also be described as a one-parameter family of deformations by defining

$$\boldsymbol{\phi} : \bar{\mathcal{R}} \times \mathbb{R} \rightarrow \mathcal{E} \quad (4)$$

transforming the position $\bar{\mathfrak{p}}_A \equiv \mathfrak{p}(A, t_0) \in \bar{\mathcal{R}}$ of each body point $A \in \mathcal{B}$ at time t_0 into its position at time t

$$\mathfrak{p}_A(t) = \mathfrak{p}(A, t) = \boldsymbol{\phi}(\mathfrak{p}_A(t_0), t). \quad (5)$$

By $\bar{\mathcal{R}}$ we shall denote the shape of the body at a time t_0 . We call the image in \mathcal{E} of \mathfrak{p}_A the *trajectory* of the body point A . The *velocity* at time t of the point A is the vector

$$\dot{\mathfrak{p}}_A(t) := \lim_{\tau \rightarrow 0} \frac{1}{\tau} (\mathfrak{p}_A(t + \tau) - \mathfrak{p}_A(t)). \quad (6)$$

After setting a coordinate system by selecting an origin \mathfrak{o} and an orthonormal basis $\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$, a description of the motion can be given in terms of coordinates as follows

$$\mathfrak{p}_A(t) = \mathfrak{o} + x_{1A}(t)\mathbf{e}_1 + x_{2A}(t)\mathbf{e}_2 + x_{3A}(t)\mathbf{e}_3. \quad (7)$$

The expression for the velocity turns out to be

$$\begin{aligned} \dot{\mathfrak{p}}_A(t) &:= \lim_{\tau \rightarrow 0} \frac{1}{\tau} ((x_{1A}(t + \tau) - x_{1A}(t))\mathbf{e}_1 + (x_{2A}(t + \tau) - x_{2A}(t))\mathbf{e}_2 + (x_{3A}(t + \tau) - x_{3A}(t))\mathbf{e}_3) \\ &= \frac{d}{dt}x_{1A}(t)\mathbf{e}_1 + \frac{d}{dt}x_{2A}(t)\mathbf{e}_2 + \frac{d}{dt}x_{3A}(t)\mathbf{e}_3. \end{aligned} \quad (8)$$

By *test velocity field* we mean the collection of the body point velocities

$$\dot{\mathfrak{p}}_A(t), \dot{\mathfrak{p}}_B(t), \dots \quad (9)$$

2 Rigid motions

A motion is *rigid* if, for any t_0 , the deformations (4) are such that for any two body points A e B and at any time t

$$\boldsymbol{\phi}(\bar{\mathfrak{p}}_B, t) = \boldsymbol{\phi}(\bar{\mathfrak{p}}_A, t) + \mathbf{R}(t)(\bar{\mathfrak{p}}_B - \bar{\mathfrak{p}}_A), \quad (10)$$

where $\mathbf{R}(t)$ is a rotation. Hence a *rigid motion* turns out to be defined by the motion of any body point, say A , and by \mathbf{R} . The corresponding expression for the velocity is

$$\dot{\boldsymbol{\phi}}(\bar{\mathfrak{p}}_B, t) = \dot{\boldsymbol{\phi}}(\bar{\mathfrak{p}}_A, t) + \dot{\mathbf{R}}(t)(\bar{\mathfrak{p}}_B - \bar{\mathfrak{p}}_A). \quad (11)$$

Replacing (10) with

$$\mathbf{p}_B(t) = \mathbf{p}_A(t) + \mathbf{R}(t)(\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A), \quad (12)$$

the velocity (11) becomes

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \dot{\mathbf{R}}(t)(\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A). \quad (13)$$

Note that from (12) we get

$$\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A = \mathbf{R}(t)^\top(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (14)$$

By substituting this expression into (13) we obtain

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \dot{\mathbf{R}}(t)\mathbf{R}(t)^\top(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (15)$$

Setting

$$\mathbf{W}(t) := \dot{\mathbf{R}}(t)\mathbf{R}(t)^\top, \quad (16)$$

allows to rewrite expression (15) as

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \mathbf{W}(t)(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (17)$$

The tensor $\mathbf{W}(t)$, called the *spin tensor*, turns out to be skew symmetric. To show this let us note that if $\mathbf{R}(t)$ is a rotation then $\mathbf{R}(t)^{-1} = \mathbf{R}(t)^\top$ is a rotation as well. Hence

$$\mathbf{R}(t)\mathbf{R}(t)^\top = \mathbf{I}. \quad (18)$$

Differentiating with respect to t we get

$$\dot{\mathbf{R}}(t)\mathbf{R}(t)^\top + \mathbf{R}(t)\dot{\mathbf{R}}(t)^\top = \mathbf{O} \quad \Rightarrow \quad \mathbf{W}(t) + \mathbf{W}(t)^\top = \mathbf{O} \quad \Rightarrow \quad \mathbf{W}(t)^\top = -\mathbf{W}(t). \quad (19)$$

Further, setting

$$\mathbf{d}(t) := \mathbf{p}_B(t) - \mathbf{p}_A(t), \quad (20)$$

from (17) we get

$$\dot{\mathbf{d}}(t) = \mathbf{W}(t)\mathbf{d}(t). \quad (21)$$

Note that by the skew symmetry of the spin

$$\dot{\mathbf{d}}(t) \cdot \mathbf{d}(t) = \mathbf{W}(t)\mathbf{d}(t) \cdot \mathbf{d}(t) = \mathbf{d}(t) \cdot \mathbf{W}(t)^\top\mathbf{d}(t) = -\mathbf{d}(t) \cdot \mathbf{W}(t)\mathbf{d}(t). \quad (22)$$

Hence

$$\dot{\mathbf{d}}(t) \cdot \mathbf{d}(t) = 0, \quad (23)$$

$$\mathbf{W}(t)\mathbf{d}(t) \cdot \mathbf{d}(t) = 0. \quad (24)$$

By the first property the velocity difference

$$\dot{\mathbf{d}}(t) = \dot{\mathbf{p}}_B(t) - \dot{\mathbf{p}}_A(t) \quad (25)$$

is either zero or orthogonal to the difference vector (20). By the second property $\mathbf{W}(t)$ transforms any vector $\mathbf{d}(t)$ into a vector orthogonal to $\mathbf{d}(t)$. A *rigid velocity field* is a velocity field satisfying (17), with $\mathbf{W}(t)$ skew symmetric.

3 Spin axis

A skew symmetric tensor $\mathbf{W}(t)$, as an endomorphism of a real vector space of dimension three, has a null eigenvalue. In fact, since the characteristic polynomial is of order three there exists at least one real eigenvalue λ . Denoting by $\mathbf{a}_o(t)$ a unit eigenvector corresponding to λ it is

$$\mathbf{W}(t)\mathbf{a}_o(t) = \lambda \mathbf{a}_o(t). \quad (26)$$

By (24)

$$\lambda = \mathbf{W}(t)\mathbf{a}_o(t) \cdot \mathbf{a}_o(t) = 0. \quad (27)$$

Hence

$$\mathbf{W}(t)\mathbf{a}_o(t) = \mathbf{o}. \quad (28)$$

Let us consider, at a time t , a line passing through $\mathbf{p}_A(t)$

$$\mathbf{c}_o(h, t) = \mathbf{p}_A(t) + h \mathbf{a}_o(t). \quad (29)$$

All body points occupying such positions have the same velocity since by (28),

$$\dot{\mathbf{c}}_o(h, t) = \dot{\mathbf{p}}_A(t) + \mathbf{W}(t)(\mathbf{c}_o(h, t) - \mathbf{p}_A(t)) = \dot{\mathbf{p}}_A(t) + h\mathbf{W}(t)\mathbf{a}_o(t) = \dot{\mathbf{p}}_A(t). \quad (30)$$

This property holds for any line parallel to $\mathbf{a}_o(t)$. Hence for each line parallel to $\mathbf{a}_o(t)$ there is a common velocity, possibly different from line to line. Let us consider now any two body points A e B and the difference vector (20). Note that the velocity difference (25) is such that, by (28),

$$\dot{\mathbf{d}}(t) \cdot \mathbf{a}_o(t) = \mathbf{W}(t)\mathbf{d}(t) \cdot \mathbf{a}_o(t) = \mathbf{d}(t) \cdot \mathbf{W}(t)^\top \mathbf{a}_o(t) = -\mathbf{d}(t) \cdot \mathbf{W}(t)\mathbf{a}_o(t) = 0. \quad (31)$$

Hence the velocity difference is either zero or orthogonal to $\mathbf{d}(t)$, by (23), and to $\mathbf{a}_o(t)$ as well. Property (31) can be also given a different interpretation. If it is put in the form

$$(\dot{\mathbf{p}}_B(t) - \dot{\mathbf{p}}_A(t)) \cdot \mathbf{a}_o(t) = 0, \quad (32)$$

it implies that

$$\dot{\mathbf{p}}_B(t) \cdot \mathbf{a}_o(t) = \dot{\mathbf{p}}_A(t) \cdot \mathbf{a}_o(t), \quad (33)$$

Thus the orthogonal projection of the velocity on $\mathbf{a}_o(t)$ turns out to be the same for all body points. Hence the velocity of each body point can be decomposed into the sum of a velocity $\mathbf{v}_o(t)$ parallel to the axis $\mathbf{a}_o(t)$, which is unique for the whole body, and a velocity orthogonal to $\mathbf{a}_o(t)$.

Let us consider a straight line passing through $\mathbf{p}_A(t)$ and lying on a plane orthogonal to $\mathbf{a}_o(t)$

$$\mathbf{c}(h, t) = \mathbf{p}_A(t) + h\mathbf{d}(t), \quad \mathbf{d}(t) \cdot \mathbf{a}_o(t) = 0. \quad (34)$$

Velocities along this line can be expressed as

$$\dot{\mathbf{c}}(h, t) = \dot{\mathbf{p}}_A(t) + h\mathbf{W}(t)\mathbf{d}(t) = \mathbf{v}_o(t) + \mathbf{v}_A^\perp(t) + h\mathbf{W}(t)\mathbf{d}(t), \quad (35)$$

with

$$\mathbf{v}_o(t) := (\dot{\mathbf{p}}_A(t) \cdot \mathbf{a}_o(t))\mathbf{a}_o(t), \quad (36)$$

$$\mathbf{v}_A^\perp(t) := (\dot{\mathbf{p}}_A(t) - \mathbf{v}_o(t)), \quad (37)$$

where $\mathbf{v}_A^\perp(t)$, like $\mathbf{d}(t)$, is a vector orthogonal to $\mathbf{a}_o(t)$.

If we choose $\mathbf{d}(t)$ orthogonal also to $\mathbf{v}_A^\perp(t)$ then $\mathbf{W}(t)\mathbf{d}(t)$, which is orthogonal both to $\mathbf{d}(t)$ and $\mathbf{a}_o(t)$ by (24) and (31), turns out to be parallel to $\mathbf{v}_A^\perp(t)$. Then there exists a unique value for h such that

$$\mathbf{v}_A^\perp(t) + h\mathbf{W}(t)\mathbf{d}(t) = \mathbf{o}, \quad (38)$$

selecting, through (34), a position where the velocity is exactly $\mathbf{v}_o(t)$, parallel to $\mathbf{a}_o(t)$. The straight line passing through this position and parallel to $\mathbf{a}_o(t)$ is called *spin axis*.

3.1 Axial vector

Since $\mathbf{W}(t)$ transforms any vector $\mathbf{d}(t)$ into a vector orthogonal both to $\mathbf{d}(t)$ and $\mathbf{a}_o(t)$, there should be a vector $\boldsymbol{\omega}(t)$ such that

$$\mathbf{W}(t)\mathbf{d}(t) = \boldsymbol{\omega}(t) \times \mathbf{d}(t) \quad \forall \mathbf{d}(t) \in \mathcal{V}. \quad (39)$$

We can prove that it exists and is unique as follows. Since

$$\mathbf{W}(t)\boldsymbol{\omega}(t) = \boldsymbol{\omega}(t) \times \boldsymbol{\omega}(t) = \mathbf{o}, \quad (40)$$

$\boldsymbol{\omega}(t)$ is an eigenvector corresponding to the eigenvalue $\lambda = 0$. Hence it belongs to the same one-dimensional eigenspace as $\mathbf{a}_o(t)$. Setting for any given orthonormal basis

$$\boldsymbol{\omega}(t) = \omega_1(t)\mathbf{e}_1 + \omega_2(t)\mathbf{e}_2 + \omega_3(t)\mathbf{e}_3, \quad (41)$$

the components are obtained through (39)

$$\begin{aligned} \mathbf{W}(t)\mathbf{e}_1 \cdot \mathbf{e}_2 &= \boldsymbol{\omega}(t) \times \mathbf{e}_1 \cdot \mathbf{e}_2 = \mathbf{e}_1 \times \mathbf{e}_2 \cdot \boldsymbol{\omega}(t) = \mathbf{e}_3 \cdot \boldsymbol{\omega}(t) \Rightarrow \omega_3(t) = \mathbf{W}(t)\mathbf{e}_1 \cdot \mathbf{e}_2 \\ \mathbf{W}(t)\mathbf{e}_2 \cdot \mathbf{e}_3 &= \boldsymbol{\omega}(t) \times \mathbf{e}_2 \cdot \mathbf{e}_3 = \mathbf{e}_2 \times \mathbf{e}_3 \cdot \boldsymbol{\omega}(t) = \mathbf{e}_1 \cdot \boldsymbol{\omega}(t) \Rightarrow \omega_1(t) = \mathbf{W}(t)\mathbf{e}_2 \cdot \mathbf{e}_3 \\ \mathbf{W}(t)\mathbf{e}_3 \cdot \mathbf{e}_1 &= \boldsymbol{\omega}(t) \times \mathbf{e}_3 \cdot \mathbf{e}_1 = \mathbf{e}_3 \times \mathbf{e}_1 \cdot \boldsymbol{\omega}(t) = \mathbf{e}_2 \cdot \boldsymbol{\omega}(t) \Rightarrow \omega_2(t) = \mathbf{W}(t)\mathbf{e}_3 \cdot \mathbf{e}_1 \end{aligned} \quad (42)$$

The vector $\boldsymbol{\omega}(t)$ is called *axial vector* of $\mathbf{W}(t)$. Relation (39) defines, through (42), an isomorphism between the space of skew symmetric tensors and the three-dimensional vector space \mathcal{V} .

3.2 Spin center

In a two-dimensional vector space, for a given rigid velocity field at time t , we call *spin center* the position of a point C such that $\dot{\mathbf{p}}_C(t) = \mathbf{o}$. Since

$$\dot{\mathbf{p}}_A(t) - \dot{\mathbf{p}}_C(t) = \mathbf{W}(t)(\mathbf{p}_A(t) - \mathbf{p}_C(t)), \quad (43)$$

if $\mathbf{p}_C(t)$ is the spin center then $\dot{\mathbf{p}}_A(t)$ equals the velocity difference and hence it is orthogonal to the line joining the placements $\mathbf{p}_A(t)$ and $\mathbf{p}_C(t)$. That is why the spin center can be obtained by the intersection of lines drawn from any two positions and orthogonal to the corresponding velocities.

4 Rigid motions in coordinate form

Let us consider a two-dimensional Euclidean space and a Cartesian coordinate system defined by an origin O and an orthonormal basis $\{\mathbf{e}_1, \mathbf{e}_2\}$. In a rigid motion the rotation $\mathbf{R}(t)$ at any time t can be described by

$$\mathbf{R}(t)\mathbf{e}_1 = \cos \theta(t)\mathbf{e}_1 + \sin \theta(t)\mathbf{e}_2, \quad (44)$$

$$\mathbf{R}(t)\mathbf{e}_2 = -\sin \theta(t)\mathbf{e}_1 + \cos \theta(t)\mathbf{e}_2. \quad (45)$$

Then the relation (10) can be transformed into the following one in terms of coordinates

$$\begin{pmatrix} x_{1B}(t) \\ x_{2B}(t) \end{pmatrix} = \begin{pmatrix} x_{1A}(t) \\ x_{2A}(t) \end{pmatrix} + \begin{pmatrix} \cos \theta(t) & -\sin \theta(t) \\ \sin \theta(t) & \cos \theta(t) \end{pmatrix} \begin{pmatrix} \bar{x}_{1B} - \bar{x}_{1A} \\ \bar{x}_{2B} - \bar{x}_{2A} \end{pmatrix}. \quad (46)$$

Differentiating with respect to t we get

$$\begin{pmatrix} \dot{x}_{1B}(t) \\ \dot{x}_{2B}(t) \end{pmatrix} = \begin{pmatrix} \dot{x}_{1A}(t) \\ \dot{x}_{2A}(t) \end{pmatrix} + \dot{\theta}(t) \begin{pmatrix} -\sin \theta(t) & -\cos \theta(t) \\ \cos \theta(t) & -\sin \theta(t) \end{pmatrix} \begin{pmatrix} \bar{x}_{1B} - \bar{x}_{1A} \\ \bar{x}_{2B} - \bar{x}_{2A} \end{pmatrix}. \quad (47)$$

Then we can replace, from (46), the expression

$$\begin{pmatrix} \bar{x}_{1B} - \bar{x}_{1A} \\ \bar{x}_{2B} - \bar{x}_{2A} \end{pmatrix} = \begin{pmatrix} \cos \theta(t) & \sin \theta(t) \\ -\sin \theta(t) & \cos \theta(t) \end{pmatrix} \begin{pmatrix} x_{1B}(t) - x_{1A}(t) \\ x_{2B}(t) - x_{2A}(t) \end{pmatrix} \quad (48)$$

into (47), thus obtaining

$$\begin{pmatrix} \dot{x}_{1B}(t) \\ \dot{x}_{2B}(t) \end{pmatrix} = \begin{pmatrix} \dot{x}_{1A}(t) \\ \dot{x}_{2A}(t) \end{pmatrix} + \begin{pmatrix} 0 & -\dot{\theta}(t) \\ \dot{\theta}(t) & 0 \end{pmatrix} \begin{pmatrix} x_{1B}(t) - x_{1A}(t) \\ x_{2B}(t) - x_{2A}(t) \end{pmatrix}. \quad (49)$$

This is the expression relating the components of the velocities in (17). Hence the matrix in (49) is the matrix of $\mathbf{W}(t)$.

In general, in a three-dimensional Euclidean space endowed with a Cartesian coordinate system whose orthonormal vector basis is $\{\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3\}$, the relation (17) can be transformed into the following one in terms of coordinates

$$\begin{pmatrix} \dot{x}_{1B}(t) \\ \dot{x}_{2B}(t) \\ \dot{x}_{3B}(t) \end{pmatrix} = \begin{pmatrix} \dot{x}_{1A}(t) \\ \dot{x}_{2A}(t) \\ \dot{x}_{3A}(t) \end{pmatrix} + \begin{pmatrix} 0 & -\omega_3(t) & \omega_2(t) \\ \omega_3(t) & 0 & -\omega_1(t) \\ -\omega_2(t) & \omega_1(t) & 0 \end{pmatrix} \begin{pmatrix} x_{1B}(t) - x_{1A}(t) \\ x_{2B}(t) - x_{2A}(t) \\ x_{3B}(t) - x_{3A}(t) \end{pmatrix}. \quad (50)$$

The matrix of \mathbf{W} is skew symmetric because

$$\mathbf{W}^T = -\mathbf{W} \quad \Rightarrow \quad \mathbf{W}\mathbf{e}_i \cdot \mathbf{e}_j = -\mathbf{e}_i \cdot \mathbf{W}\mathbf{e}_j. \quad (51)$$

5 Affine motion

A motion is said to be *affine* if the one-parameter family of deformations (4) is such that for any two body points A and B and for any t

$$\boldsymbol{\phi}(\bar{\mathbf{p}}_B, t) = \boldsymbol{\phi}(\bar{\mathbf{p}}_A, t) + \mathbf{F}(t)(\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A), \quad (52)$$

where $\mathbf{F}(t)$ is a tensor such that $\det \mathbf{F}(t) > 0$. Hence an *affine motion* is defined by the motion of any body point, say A, and by the values of the *deformation gradient* $\mathbf{F}(t)$.

The velocity field in an affine motion is given by

$$\dot{\boldsymbol{\phi}}(\bar{\mathbf{p}}_B, t) = \dot{\boldsymbol{\phi}}(\bar{\mathbf{p}}_A, t) + \dot{\mathbf{F}}(t)(\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A). \quad (53)$$

Replacing (52) with

$$\mathbf{p}_B(t) = \mathbf{p}_A(t) + \mathbf{F}(t)(\bar{\mathbf{p}}_B - \bar{\mathbf{p}}_A), \quad (54)$$

we get

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \dot{\mathbf{F}}(t)(\mathbf{p}_B(t_0) - \mathbf{p}_A(t_0)). \quad (55)$$

Since from (54)

$$\mathbf{p}_B(t_0) - \mathbf{p}_A(t_0) = \mathbf{F}(t)^{-1}(\mathbf{p}_B(t) - \mathbf{p}_A(t)), \quad (56)$$

then

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \dot{\mathbf{F}}(t)\mathbf{F}(t)^{-1}(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (57)$$

Setting

$$\mathbf{L}(t) := \dot{\mathbf{F}}(t)\mathbf{F}(t)^{-1}, \quad (58)$$

the expression (57) can be written

$$\dot{\mathbf{p}}_B(t) = \dot{\mathbf{p}}_A(t) + \mathbf{L}(t)(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (59)$$

If we consider a deformation transforming positions at time t into positions at time $t + \tau$

$$\boldsymbol{\phi}_t(\mathbf{p}_B(t), \tau) = \boldsymbol{\phi}_t(\mathbf{p}_A(t), \tau) + \mathbf{F}_t(\tau)(\mathbf{p}_B(t) - \mathbf{p}_A(t)), \quad (60)$$

we get the following expression for the velocities at time t

$$\dot{\boldsymbol{\phi}}_t(\mathbf{p}_B(t), 0) = \dot{\boldsymbol{\phi}}_t(\mathbf{p}_A(t), 0) + \dot{\mathbf{F}}_t(0)(\mathbf{p}_B(t) - \mathbf{p}_A(t)). \quad (61)$$

By comparing this expression with (59) we obtain

$$\mathbf{L}(t) = \dot{\mathbf{F}}(t)\mathbf{F}(t)^{-1} = \dot{\mathbf{F}}_t(0). \quad (62)$$

This expression allows us to give a useful characterization of \mathbf{L} . From the polar decomposition of the deformation gradient

$$\mathbf{F}_t(\tau) = \mathbf{R}_t(\tau)\mathbf{U}_t(\tau) \quad (63)$$

we get, differentiating with respect to time at $\tau = 0$,

$$\mathbf{L}(t) = \dot{\mathbf{F}}_t(0) = \dot{\mathbf{R}}_t(0)\mathbf{U}_t(0) + \mathbf{R}_t(0)\dot{\mathbf{U}}_t(0) = \dot{\mathbf{R}}_t(0) + \dot{\mathbf{U}}_t(0), \quad (64)$$

since $\mathbf{F}_t(0) = \mathbf{I}$ implies $\mathbf{R}_t(0) = \mathbf{I}$ and $\mathbf{U}_t(0) = \mathbf{I}$. Note that $\dot{\mathbf{R}}_t(0)$ is skew symmetric while $\dot{\mathbf{U}}_t(0)$ is symmetric, since

$$\begin{aligned} \mathbf{R}_t(\tau)^\top \mathbf{R}_t(\tau) = \mathbf{I} &\Rightarrow \dot{\mathbf{R}}_t(\tau)^\top \mathbf{R}_t(\tau) + \mathbf{R}_t(\tau)^\top \dot{\mathbf{R}}_t(\tau) = \mathbf{O} \\ &\Rightarrow \dot{\mathbf{R}}_t(0)^\top + \dot{\mathbf{R}}_t(0) = \mathbf{O}, \end{aligned} \quad (65)$$

$$\dot{\mathbf{U}}_t(\tau)^\top = \dot{\mathbf{U}}_t(\tau) \Rightarrow \dot{\mathbf{U}}_t(0)^\top = \dot{\mathbf{U}}_t(0). \quad (66)$$

If we consider the decomposition of $\mathbf{L}(t)$

$$\mathbf{L}(t) = \mathbf{D}(t) + \mathbf{W}(t), \quad (67)$$

with

$$\mathbf{D}(t) := \frac{1}{2}(\mathbf{L}(t) + \mathbf{L}(t)^\top), \quad \mathbf{W}(t) := \frac{1}{2}(\mathbf{L}(t) - \mathbf{L}(t)^\top) \quad (68)$$

it turns out that

$$\mathbf{D}(t) = \dot{\mathbf{U}}_t(0), \quad \mathbf{W}(t) = \dot{\mathbf{R}}_t(0). \quad (69)$$

This is the reason why $\mathbf{D}(t)$ and $\mathbf{W}(t)$ are called *stretching* and *spin* respectively.

An *affine velocity field* is a velocity field whose velocities are given by (59), where $\mathbf{L}(t)$ is a tensor.

6 Velocity gradient

A generic motion at any time t can be described by a deformation

$$\boldsymbol{\phi}(\cdot, t) : \bar{\mathcal{R}} \mapsto \mathcal{E}. \quad (70)$$

Let us consider a straight line

$$\bar{c}(h) = \bar{\rho}_A + h \bar{\mathbf{d}} \quad (71)$$

on the shape $\bar{\mathcal{R}}$ and for each time t the curve $c(\cdot, t)$ on \mathcal{R} such that

$$c(h, t) = \boldsymbol{\phi}(\bar{c}(h), t). \quad (72)$$

The tangent vector at $c(0, t)$ is defined as the limit

$$\mathbf{d}(t) := \lim_{h \rightarrow 0} \frac{1}{h} (c(h, t) - c(0, t)). \quad (73)$$

At each time t we can define, for each body point A, the gradient of the vector field $\boldsymbol{\phi}(\cdot, t)$ as the tensor such that

$$\mathbf{F}(\bar{\rho}_A, t) : \bar{\mathbf{d}} \mapsto \mathbf{d}(t), \quad (74)$$

transforming vectors which are tangent to curves passing through $\bar{\rho}_A$ into vectors which are tangent to the corresponding curves through $\rho_A(t) = \boldsymbol{\phi}(\bar{\rho}_A, t)$.

At time t the velocity of body point is given by

$$\mathbf{v}_t : \rho_A(t) \mapsto \dot{\rho}_A(t). \quad (75)$$

whose domain is the shape of the body at time t and which is called *spatial velocity field*. The gradient of this vector field [see APPENDIX 2] is the tensor $\nabla_{\mathbf{v}_t}$ such that

$$\nabla_{\mathbf{v}_t} \mathbf{d}(t) = \lim_{h \rightarrow 0} \frac{1}{h} (\mathbf{v}_t(c(h, t)) - \mathbf{v}_t(c(0, t))) = \lim_{h \rightarrow 0} \frac{1}{h} (\dot{c}(h, t) - \dot{c}(0, t)). \quad (76)$$

Since from (73)

$$\dot{\mathbf{d}}(t) = \lim_{h \rightarrow 0} \frac{1}{h} (\dot{c}(h, t) - \dot{c}(0, t)), \quad (77)$$

we get from (76)

$$\nabla_{\mathbf{v}_t} \mathbf{d}(t) = \dot{\mathbf{d}}(t). \quad (78)$$

From (74) we get also

$$\dot{\mathbf{d}}(t) = \lim_{\tau \rightarrow 0} \frac{1}{\tau} (\mathbf{d}(t + \tau) - \mathbf{d}(t)) = \dot{\mathbf{F}}(\bar{\rho}_A, t) \bar{\mathbf{d}} = \dot{\mathbf{F}}(\bar{\rho}_A, t) \mathbf{F}(\bar{\rho}_A, t)^{-1} \mathbf{d}(t). \quad (79)$$

Replacing this expression into (78) it turns out, dropping function arguments out,

$$\nabla_{\mathbf{v}_t} = \dot{\mathbf{F}} \mathbf{F}^{-1}. \quad (80)$$

If we consider the deformation from the shape at a fixed time t to any time $t + \tau$

$$\boldsymbol{\phi}_t(\cdot, \tau) : \rho_A(t) \mapsto \rho_A(t + \tau), \quad (81)$$

we can define, for each body point A, the gradient of $\boldsymbol{\phi}_t(\cdot, \tau)$, as the tensor

$$\mathbf{F}_t(\rho_A(t), \tau) : \mathbf{d}(t) \mapsto \mathbf{d}(t + \tau), \quad (82)$$

transforming vectors which are tangent to curves through $\rho_A(t)$ into vectors tangent to the corresponding curves through $\rho_A(t + \tau)$. Instead of (79) we get

$$\dot{\mathbf{d}}(t) = \lim_{\tau \rightarrow 0} \frac{1}{\tau} (\mathbf{d}(t + \tau) - \mathbf{d}(t)) = \dot{\mathbf{F}}_t(\rho_A(t), t) \mathbf{d}(t) \quad (83)$$

and finally

$$\nabla \mathbf{v}_t = \dot{\mathbf{F}}_t. \quad (84)$$

7 Affine velocity fields

The meaning of the velocity gradient can be illustrated in the following way. In a two-dimensional space let us consider a body in the shape of a square at a time t . Let us consider also an orthonormal basis whose vectors are parallel to the sides of the square and denote the matrix of the velocity gradient by

$$\begin{pmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{pmatrix} \quad (85)$$

The velocity field is described by (59). The shape the body takes in a sufficiently short time interval τ can be described by the expression

$$\begin{aligned} \rho_B(t + \tau) &= \rho_B(t) + \dot{\rho}_B(t)\tau + \mathbf{o}(\tau) \\ &= \rho_B(t) + (\dot{\rho}_O(t) + \mathbf{L}(t)(\rho_B(t) - \rho_O(t)))\tau + \mathbf{o}(\tau) \end{aligned} \quad (86)$$

If we assume that the center is at rest ($\dot{\rho}_O(t) = 0$) we get

$$\rho_B(t + \tau) = \rho_B(t) + \mathbf{L}(t)(\rho_B(t) - \rho_O(t))\tau + \mathbf{o}(\tau). \quad (87)$$

Figures 1, 2, 3, show the shapes the body takes according to the values of $\mathbf{L}(t)$ given by the matrices in the tables below arranged in the same order as the shapes

Fig. 1

$\begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix}$
$\begin{pmatrix} 0 & 0 \\ 1 & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}$

Fig. 2

$\begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & \frac{1}{2} \\ \frac{1}{2} & 0 \end{pmatrix}$
$\begin{pmatrix} 0 & \frac{1}{2} \\ \frac{1}{2} & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & 0 \\ 0 & 1 \end{pmatrix}$

Fig. 3

$\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & \frac{1}{2} \\ -\frac{1}{2} & 0 \end{pmatrix}$
$\begin{pmatrix} 0 & -\frac{1}{2} \\ \frac{1}{2} & 0 \end{pmatrix}$	$\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$

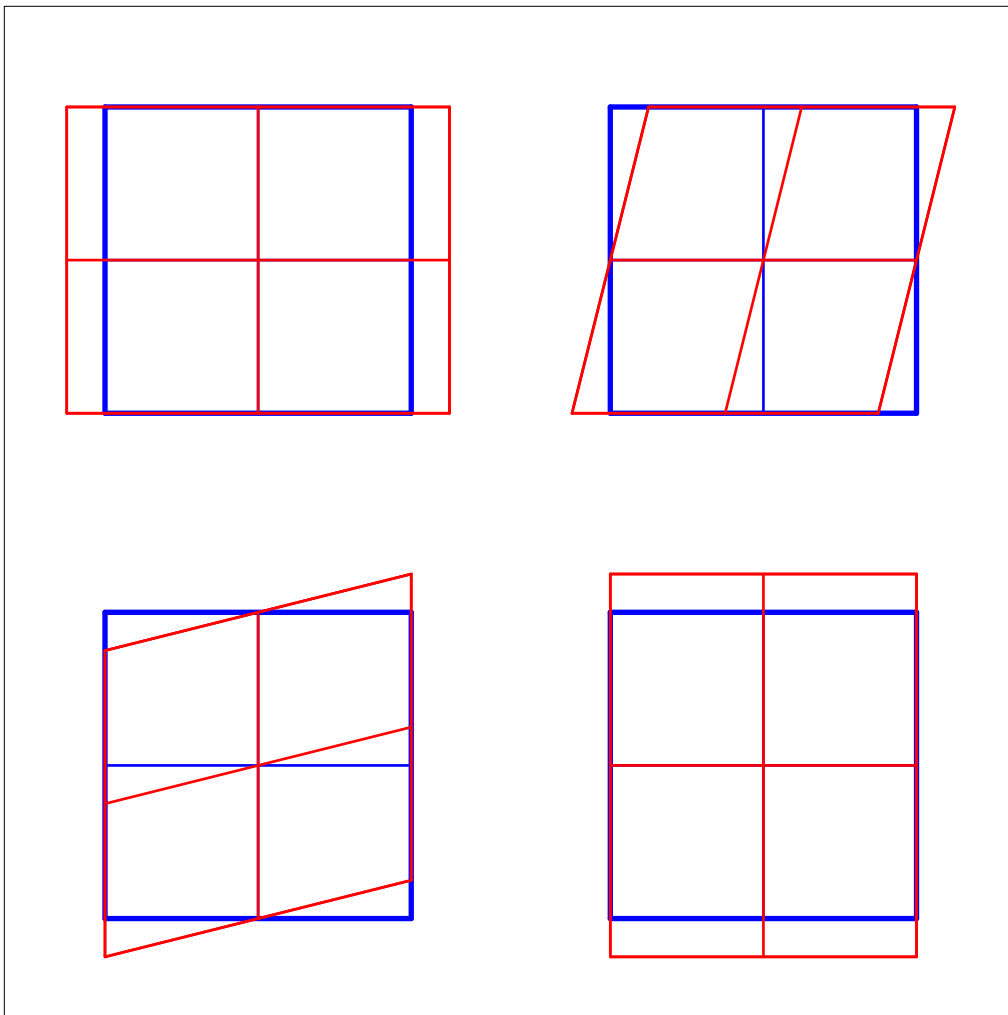


Figure 1: Illustration of the velocity gradient

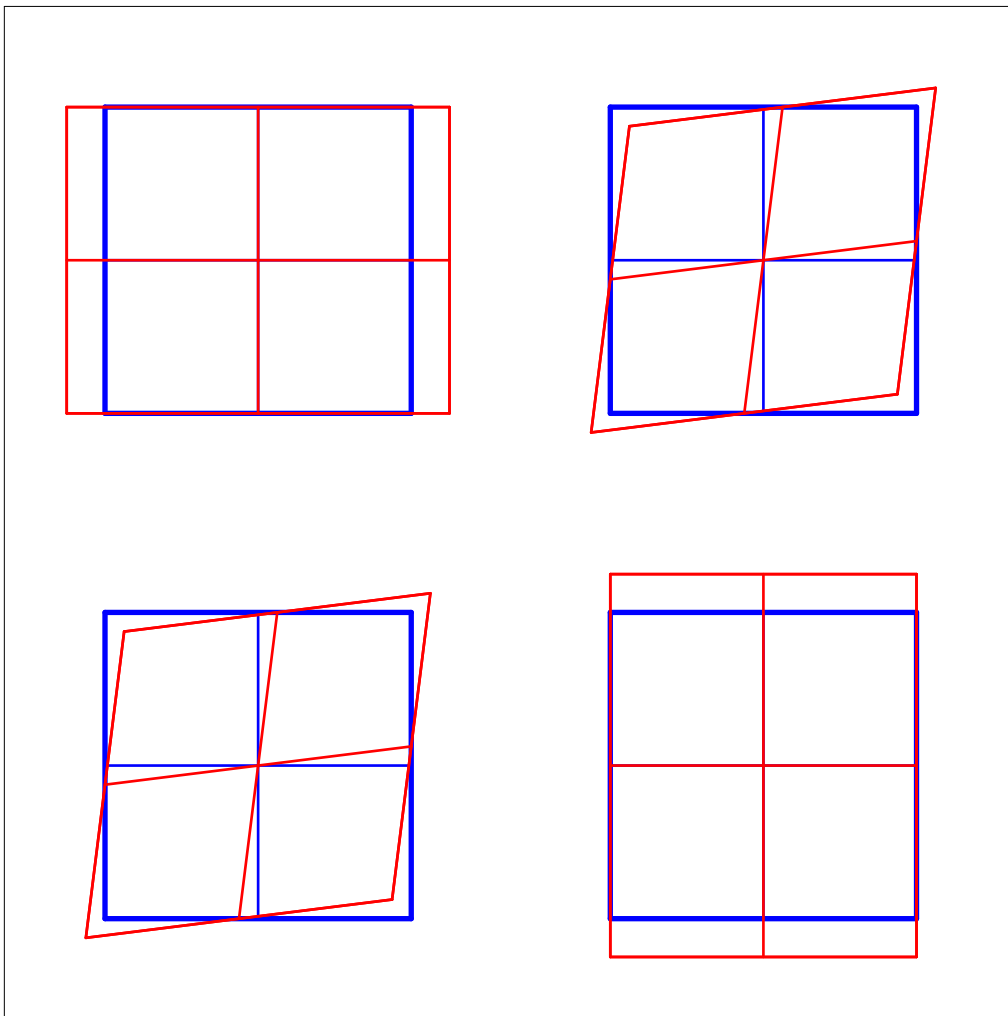


Figure 2: Illustration of the velocity gradient (symmetric part)

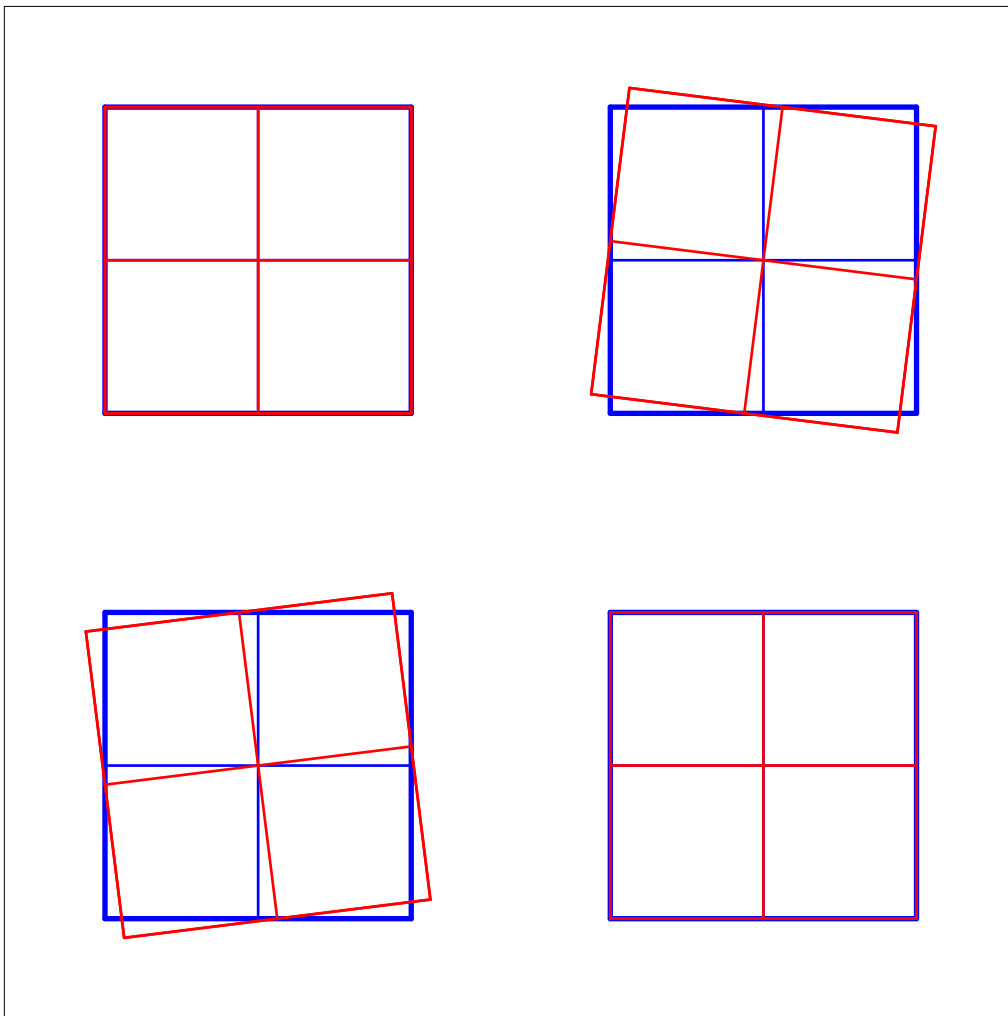


Figure 3: Illustration of the velocity gradient (skew symmetric part)