

Displacement field u

$$u(x) = \phi(x) - x$$

$$\nabla u e = \lim_{h \rightarrow 0} \frac{u(\bar{c}(h)) - u(\bar{c}(0))}{h} \quad \bar{c}'(0) = e$$

$$= \lim_{h \rightarrow 0} \frac{(\phi(\bar{c}(h)) - \bar{c}(h)) - (\phi(\bar{c}(0)) - \bar{c}(0))}{h}$$

$$= \lim_{h \rightarrow 0} \frac{\phi(\bar{c}(h)) - \phi(\bar{c}(0))}{h} - \lim_{h \rightarrow 0} \frac{\bar{c}(h) - \bar{c}(0)}{h}$$

$$= \lim_{h \rightarrow 0} \frac{c(h) - c(0)}{h} - \lim_{h \rightarrow 0} \frac{\bar{c}(h) - \bar{c}(0)}{h}$$

$$= c'(0) - \bar{c}'(0) = F\bar{c}'(0) - \bar{c}'(0) = (F - I)e$$

$$\Rightarrow \nabla u = F - I, \quad F = I + \nabla u$$

$$[\nabla u] = \begin{pmatrix} u_{1,1} & u_{1,2} & u_{1,3} \\ u_{2,1} & u_{2,2} & u_{2,3} \\ u_{3,1} & u_{3,2} & u_{3,3} \end{pmatrix}$$

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$$\int_V \mathbf{S} \cdot \nabla \mathbf{r} dV$$

$$\mathbf{S} = \hat{\mathbf{S}}_e(\mathbf{F}) + \mathbf{S}^+$$

$$\mathbf{S}^+ = (\det \mathbf{F}) \mathbf{T}^+ \mathbf{F}^{-T}$$

$$\mathbf{T} = \hat{\mathbf{T}}_e(\mathbf{F}) + \mathbf{T}^+$$

$$\mathbf{T}^+ = 2\mu \operatorname{sym}(\dot{\mathbf{F}}\mathbf{F}^{-1})$$

$$\hat{\mathbf{T}}_e(\mathbf{F}) = 2k_I J^{-\frac{5}{3}} \left(\mathbf{B} - \frac{1}{3} I_1 \mathbf{I} \right) + 2k_V (J-1)$$

$$\hat{\mathbf{S}}_e(\mathbf{F}) = 2k_I J^{-\frac{2}{3}} \left(\mathbf{F} - \frac{1}{3} I_1 \mathbf{F}^{-T} \right) + 2k_V (J-1) J \mathbf{F}^{-T}$$

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$$\int_{\mathcal{F}_1} p e_1 dA = \int_{\mathcal{F}_1} p a_1 dA$$

$$\bar{p} = p \frac{A_{\mathcal{F}_1}}{A_{\mathcal{F}_1}}$$

$$\int_{\mathcal{F}_1} dA = \int_{\mathcal{F}_1} a dA$$

$$a_1 = \frac{A_{\mathcal{F}_1}}{A_{\mathcal{F}_1}} = \|(\text{col } F) e_1\| = \left(cF_{11}^2 + cF_{21}^2 + cF_{31}^2 \right)^{1/2}$$

$$\bar{p} = p a_1$$

uni-axial deformation

$$\left\{ \begin{array}{l} \frac{p}{2k_I} = J \left(\lambda^2 - \frac{1}{\lambda} \right) \\ J = 1 + \frac{1}{3} \frac{p}{2k_V} \end{array} \right. \quad \begin{array}{l} p \text{ traction per unit current area} \\ 2k_I \text{ shear modulus} \\ 2k_V \text{ bulk modulus} \end{array}$$

CONSOL:

\bar{p} : traction to be applied (as a "weak contribution")

compare u_1 at the centre of face \mathcal{F}_1

to λk_1 (as a solution to the uniaxial problem)

	001	001a	001b (fine)	001c (coarse)
k_I	5 GPa	5 GPa		
k_V	50 GPa	50 GPa		
L	0.005	0.005		
R	$L/4$	$L/4$		
u_1/L	-0.25	-0.3159	-0.3148	-0.3158
λ	0.75	0.6839	0.6853	0.6845

$$\lambda = 0.67257$$

$$(L + u_1) = \lambda L$$

$$u_1 = (\lambda - 1)L$$

$$u_1/L = (\lambda - 1)$$

ρ face per unit current area

$\bar{\rho}$ face per unit reference area

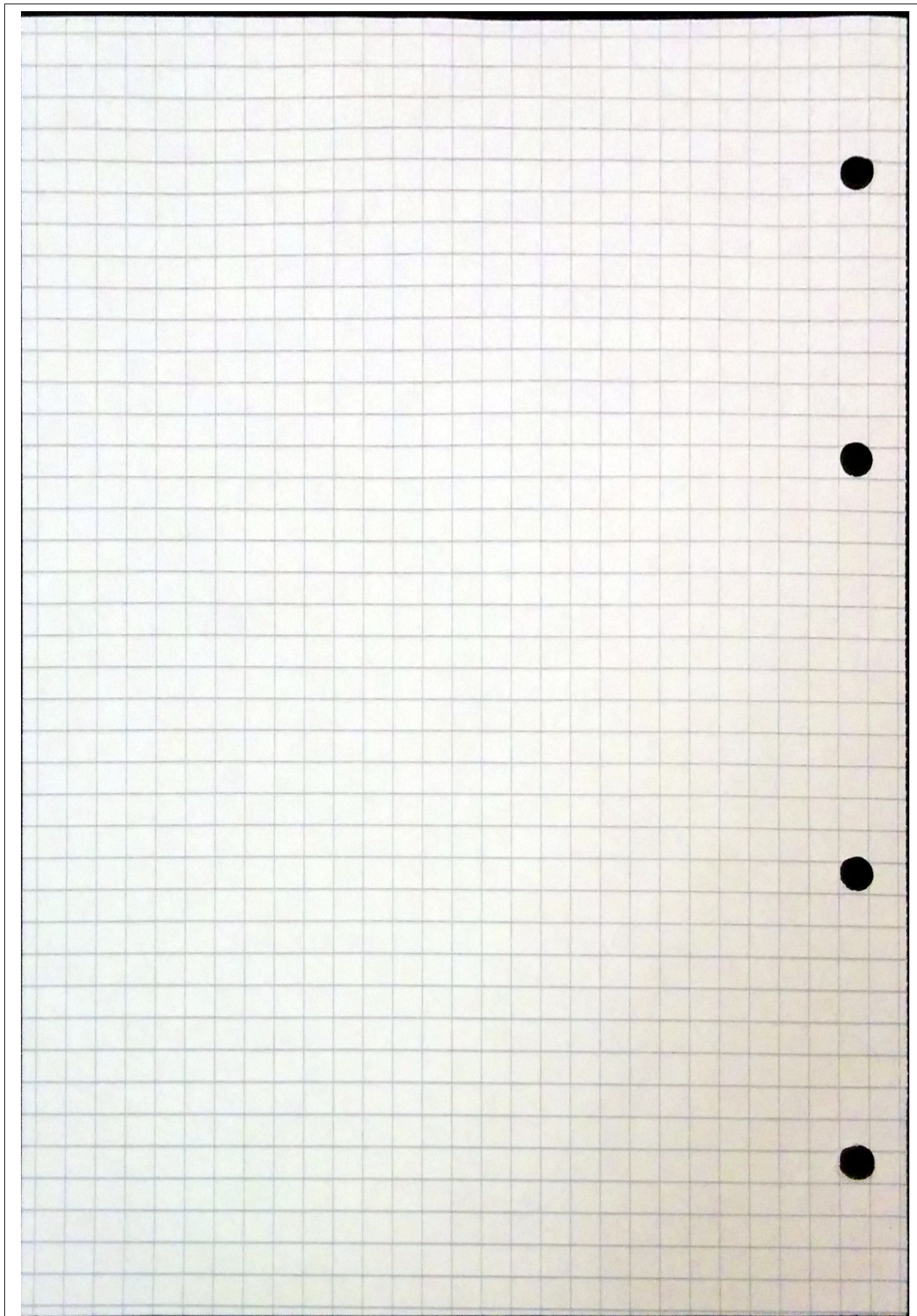
$$\bar{\rho} = \rho \frac{A_F}{A_E}$$

CONSOL

	field	test field
u	u_1 u_2 u_3	v test (u_1) test (u_2) test (u_3)
	$1+u_1x$ u_1y u_1z	
F	u_2x $1+u_2y$ u_2z	
	u_3x u_3y $1+u_3z$	
	u_1xt u_1yt u_1zt	
\dot{F}	u_2xt u_2yt u_2zt	
	u_3xt u_3yt u_3zt	

- The space of test velocity fields is isomorphic to the space of displacement fields.
- The space of test velocity gradients is, as a consequence, isomorphic to the space of displacement field gradients.

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class_consol-model-(15-01).txt      Mon Jun 08 15:24:40 2015      1
1: Dp11      1+u1x
2: Dp21      u2x
3: Dp31      u3x
4: Dp12      u1y
5: Dp22      1+u2y
6: Dp32      u3y
7: Dp13      u1z
8: Dp23      u2z
9: Dp33      1+u3z
10: f11      Dp11
11: f21      Dp21
12: f31      Dp31
13: f12      Dp12
14: f22      Dp22
15: f32      Dp32
16: f13      Dp13
17: f23      Dp23
18: f33      Dp33
19: B11      f11*f11+f12*f12+f13*f13
20: B12      f11*f21+f12*f22+f13*f23
21: B13      f11*f31+f12*f32+f13*f33
22: B21      f21*f11+f22*f12+f23*f13
23: B22      f21*f21+f22*f22+f23*f23
24: B23      f21*f31+f22*f32+f23*f33
25: B31      f31*f11+f32*f12+f33*f13
26: B32      f31*f21+f32*f22+f33*f23
27: B33      f31*f31+f32*f32+f33*f33
28: detF     -(f13*f22*f31)+f12*f23*f31+f13*f21*f32-f11*f23*f32-f12*f21*f33+f11*f22*f33
29: J        detF
30: i1       B11+B22+B33
31: i2       (i1^2-(B11^2+B12^2+B13^2+B21^2+B22^2+B23^2+B31^2+B32^2+B33^2))/2
32: cfF11    -(f23*f32)+f22*f33
33: cfF12    f23*f31-f21*f33
34: cfF13    -(f22*f31)+f21*f32
35: cfF21    f13*f32-f12*f33
36: cfF22    -(f13*f31)+f11*f33
37: cfF23    f12*f31-f11*f32
38: cfF31    -(f13*f22)+f12*f23
39: cfF32    f13*f21-f11*f23
40: cfF33    -(f12*f21)+f11*f22
41: cfDp11   cfF11
42: cfDp21   cfF21
43: cfDp31   cfF31
44: cfDp12   cfF12
45: cfDp22   cfF22
46: cfDp32   cfF32
47: cfDp13   cfF13
48: cfDp23   cfF23
49: cfDp33   cfF33
50: finv11   cfF11/detF
51: finv21   cfF12/detF
52: finv31   cfF13/detF
53: finv12   cfF21/detF
54: finv22   cfF22/detF
55: finv32   cfF23/detF
56: finv13   cfF31/detF
57: finv23   cfF32/detF
58: finv33   cfF33/detF
59: f11t     u1xt
60: f21t     u2xt
61: f31t     u3xt
62: f12t     u1yt
63: f22t     u2yt
64: f32t     u3yt
65: f13t     u1zt
66: f23t     u2zt
67: f33t     u3zt
68: Dv11     f11t*finv11+f12t*finv21+f13t*finv31
69: Dv21     f21t*finv11+f22t*finv21+f23t*finv31
70: Dv31     f31t*finv11+f32t*finv21+f33t*finv31

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class_consol-model-(15-01).txt

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71: Dv12  f11t*finv12+f12t*finv22+f13t*finv32
72: Dv22  f21t*finv12+f22t*finv22+f23t*finv32
73: Dv32  f31t*finv12+f32t*finv22+f33t*finv32
74: Dv13  f11t*finv13+f12t*finv23+f13t*finv33
75: Dv23  f21t*finv13+f22t*finv23+f23t*finv33
76: Dv33  f31t*finv13+f32t*finv23+f33t*finv33
77: S11   (Se11+Sdiss11)
78: S21   (Se21+Sdiss21)
79: S31   (Se31+Sdiss31)
80: S12   (Se12+Sdiss12)
81: S22   (Se22+Sdiss22)
82: S32   (Se32+Sdiss32)
83: S13   (Se13+Sdiss13)
84: S23   (Se23+Sdiss23)
85: S33   (Se33+Sdiss33)
86: Se11  2*kI*J^(-2/3)*(f11-(i1/3)*finv11)+2*kV*(J-1)*cfF11
87: Se12  2*kI*J^(-2/3)*(f12-(i1/3)*finv21)+2*kV*(J-1)*cfF12
88: Se13  2*kI*J^(-2/3)*(f13-(i1/3)*finv31)+2*kV*(J-1)*cfF13
89: Se21  2*kI*J^(-2/3)*(f21-(i1/3)*finv12)+2*kV*(J-1)*cfF21
90: Se22  2*kI*J^(-2/3)*(f22-(i1/3)*finv22)+2*kV*(J-1)*cfF22
91: Se23  2*kI*J^(-2/3)*(f23-(i1/3)*finv32)+2*kV*(J-1)*cfF23
92: Se31  2*kI*J^(-2/3)*(f31-(i1/3)*finv13)+2*kV*(J-1)*cfF31
93: Se32  2*kI*J^(-2/3)*(f32-(i1/3)*finv23)+2*kV*(J-1)*cfF32
94: Se33  2*kI*J^(-2/3)*(f33-(i1/3)*finv33)+2*kV*(J-1)*cfF33
95: Sdiss11 cfF11*Tdiss11+cfF21*Tdiss12+cfF31*Tdiss13
96: Sdiss12 cfF12*Tdiss11+cfF22*Tdiss12+cfF32*Tdiss13
97: Sdiss13 cfF13*Tdiss11+cfF23*Tdiss12+cfF33*Tdiss13
98: Sdiss21 cfF11*Tdiss21+cfF21*Tdiss22+cfF31*Tdiss23
99: Sdiss22 cfF12*Tdiss21+cfF22*Tdiss22+cfF32*Tdiss23
100: Sdiss23 cfF13*Tdiss21+cfF23*Tdiss22+cfF33*Tdiss23
101: Sdiss31 cfF11*Tdiss31+cfF21*Tdiss32+cfF31*Tdiss33
102: Sdiss32 cfF12*Tdiss31+cfF22*Tdiss32+cfF32*Tdiss33
103: Sdiss33 cfF13*Tdiss31+cfF23*Tdiss32+cfF33*Tdiss33
104: T11   (Te11+Tdiss11)
105: T21   (Te21+Tdiss21)
106: T31   (Te31+Tdiss31)
107: T12   (Te12+Tdiss12)
108: T22   (Te22+Tdiss22)
109: T32   (Te32+Tdiss32)
110: T13   (Te13+Tdiss13)
111: T23   (Te23+Tdiss23)
112: T33   (Te33+Tdiss33)
113: Te11  2*kI*J^(-5/3)*(B11-i1/3)+2*kV*(J-1)
114: Te12  2*kI*J^(-5/3)*B12
115: Te13  2*kI*J^(-5/3)*B13
116: Te21  2*kI*J^(-5/3)*B21
117: Te22  2*kI*J^(-5/3)*(B22-i1/3)+2*kV*(J-1)
118: Te23  2*kI*J^(-5/3)*B23
119: Te31  2*kI*J^(-5/3)*B31
120: Te32  2*kI*J^(-5/3)*B32
121: Te33  2*kI*J^(-5/3)*(B33-i1/3)+2*kV*(J-1)
122: Tdiss11 mu*(Dv11+Dv11)
123: Tdiss12 mu*(Dv12+Dv21)
124: Tdiss13 mu*(Dv13+Dv31)
125: Tdiss21 mu*(Dv21+Dv12)
126: Tdiss22 mu*(Dv22+Dv22)
127: Tdiss23 mu*(Dv23+Dv32)
128: Tdiss31 mu*(Dv31+Dv13)
129: Tdiss32 mu*(Dv32+Dv23)
130: Tdiss33 mu*(Dv33+Dv33)
131: TSph  (T11+T22+T33)/3
132: phi  kI*(J^(-2/3)*i1-3)+kV*(J-1)^2

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